AFML-TR-74-250 Part IV

DIELECTRIC CONSTANT AND LOSS DAYA

Laboratory for Insulation Research Massachusetts Institute of Technology Cambridge, MA 02139

December 1980

FINAL REPORT AFML-TR-74-250, PART IV
INTERIM REPORT FOR PERIOD JANUARY 1977 - MAY 1980

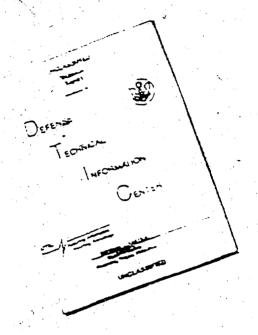
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REPORT DOCUMENTATION	READ INSTRUCTIONS BEFORE COMPLETING FORM				
1. REPORT NUMBER		3. RECIPIENT'S CATALOG HUMBER			
AFML-TR-74-250, Part IV	AD-A7-2	2001			
4. TITLE (and Subtitle)		S. TYPE CE PE THE A PERIOD COVERED			
		Final Report for period			
DIELECTRIC CONSTANT AND LOSS DAT	y _A	1 Jan 1977 - 15 May 1980			
DIDIENTIAL CONSTRAIN THE BODG BILL	•	6. PEMFORMING ORG. REPORT NUMBER			
7. AUTHOR(a)		8. CONTRACT OR GRANT NUMBER(#)			
William B. Westphal		F33615-77-C-5063			
9. PERFORMING ORGANIZATION NAME AND ADDRESS		10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS			
		Project 2423 01 04			
		1 201862 2423 01 04			
11. CONTROLLING OFFICE NAME AND ADDRESS		12. REPORT DATE			
Laboratory for Insulation Resear	ch	December 1980			
Massachusetts Institute of Wechn		13. NUMBER OF PAGES			
Cambridge, MA 02139		85			
14. MONITORING AGENCY NAME & ADDRESS(II dilleren	•	18. SECURITY CLASS. (of this teport)			
Materials Laboratory (AFWAL/MLPS AF Wright Aeronautical Laborator	-	Unclassified			
Wright-Patterson AFB, OH 45433		15a, DECLASSIFICATION/DOWNGRADING SCHEDULE			
16. DISTRIBUTION STATEMENT (of this Report)					
Approved for public release; distribution unlimited					
17. DISTRIBUTION STATEMENT (of the abstract entered in Block 20, if different from Report)					
18. SUPPLEMENTARY NOTES	18. SUPPLEMENTARY NOTES				
19. KEY WORDS (Continue on reverse side if necessary an	d identify by block number)				
High-temperature materials, Inorganics, Liquids, Minerals, Organics, Plastics					
20. ABSTRACT (Continue on reverse side if necessary and	I identify by block number)				
The main body of this report lists dielectric constant and loss data on materials measured in this laboratory in the period 1 July 1977 through 15 May 1980 together with measurements techniques and calculations.					
The index following the data section is intended to be a complete reference to dielectric measurement data of this laboratory to date.					

PREFACE

The dielectric constant and loss data presented in this report were measured at the Laboratory for Insulation Research of the Massachusetts Institute of Technology, Cambridge,

Massachusetts, by W. B. Westphal. This work was performed between 1 January 1977 and 15 May 1980 under Contract F33615-77-C-5063, Project No. 7514, Task No. 24230104 for the Materials Laboratory of the Air Force Wright Aeronautical Laboratories.

This report was submitted by the author for publication in August 1980.

The work was administered under direction of the AF Materials Laboratory, with Mr. John C. Olson (AFWAL/MLPJ) acting as project engineer.



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SUMMARY

The first sections of this report describe changes in measurement techniques and programming of calculations.

A technical report dated December 1975 presents data on materials measured in the early part of this contract. A later data report is dated May 1977. The index following the data section refers to early data reports and uses the prefix 10- for pages of the present report.

The data section does not generally include measurements on research samples under development by or for the Air Force Materials Laboratory.

MEASUREMENT TECHNIQUE

The basic measurement techniques using bridges, reentrant cavities, standing waves, and dielectric-filled cavities have been discussed in previous reports. During the present contract period the only new type of measurements has been for high loss liquids: the use of a glass or plastic capillary tube mounted in a plane one-quarter wavelength from the short in the standing wave system. The tube axis is parallel to the electric field in either rectangular or circular hollow waveguide. This method was used for water-acid solutions, liquid ammonia and sulfur.

PROGRAMMING

Program 1, in the following section, is used for calculating the dielectric constant and loss of a sample in a capillary tube. The input data:

- DS node width, sample in
- SN node position, sample in
- CONC specified acid concentration
 - NC number of measurements
 - DG node width, empty capilliary
 - GN node position, empty capilliary
 - R inner radius of capilliary
- FGH frequency, GHz
 - C conversion factor between capilliary admittance and waveguide admittance at the same plane
- Cl initial guess for correction term in Kl due to loss, Iteration finds exact correction
- WLG wavelength in air filled waveguide
- SMF conversion factor to calculate conductivity from loss factor

*References

- 1. Tech. Rep. 182 Lab. Ins. Res., Contract AF33(616)-8353, October 1963.
- 2. " " 201 " " " " October 1966.
- 3. AFML-TR-66-28, " " " AF33(615)-2199, January 1966.
- 4. AFML-TR-70-138, " " F33615-67C-1612, July 1970.
- 5. AFML-TR-71-66, " " " F33615-70C-1220, April 1971.
- AFML-TR-74-250, Pt. II, Lab. Ins. Res., Contract F33615-71-C-1274,

December 1975

7. AFML-TR-74-250, Pt. III, " " Contract F33615-75-C-5020,

May 1977

Program 1 High Loss Liquid in Capilliary

FORTRAN IV G1 RELEASE 2.0

```
0001
                           REAL+8 TWO, WL, FGH, PII3, PII4, WLG, XOG, DELN, TANG, EG, DG, XOS, GN, SN,
                          2TANS. THETA. DS.ES, K1M, K2M, K1, K2, C1, KM, KMA, KMB, K1 CAL, K2CAL, ERROR, 3WE, K1 OLD, K2OLD, EROLD, SMF, SIGMA, CONC. R, C, STEP(4)/.03D0,.01D0.
                          4.003D0,.001D0/,F(2)/1.D0,-1.D0/,FAKE(2),FUN(2),ONE
COMPLEX+16 ZONE,ZOONE,TWOC,YG,YT,KMAC,KMBC,GR,D2C,D3C,D4C,D5C
0002
                          2D6C, D7C, J11, J12, J13, J14, J1, J01, J02, J03, J04, J0, RATIO, K1C, K2C, KCOR,
                          3YG1,YG2,YG3,YG4,YT2,YT3,YT4,Y5,KC
EQUIVALENCE (FAKE(1),YS),(FUN(1),KCOR)
0003
0004
                           DIMENSION DS(40), SN(40), CONC(40), DATE(39)
0005
                           NAMELIST/IN/DS,SN,CONG,NC/CONST/DG.GN,DELN,R,FGH,C,C1,WLG,SMF
0006
                      200 FORMAT (1X, 39A2)
                      201 FORMAT(1H0,20X,39A2,/)
100 FORMAT(1X,7HWT%ACIE,5X,2HK1,3X,9HUNCOR, K1,5X,2HK2,3X,
0007
000B
                      29HUNCOR. K2,3X,12H5 GMA MHO/CM.1X,5HERROR,10X,3HJ04,10X,3HJ14)
101 FORMAT(F7.3,1X,F8.2,1X,F8.2,3X,F8.2,2X,F8.2,3X,F9.5,1X,
0009
                          2E9.2, 1X, E9. 2, 1X, E9. 2. 1X, E9. 2, 1X, E9. 2)
0010
                      102 FORMAT(5X,2HDS,10X,2HSN,10X,4HCONC,8X,1HI)
0011
                      103 FORMAT(1X,F10.4,1X,F10.4,1X,F10.4,8X,I2)
                      104 FORMAT(3X,13HKOUNT FOR K1=,1X,I2)
105 FORMAT(3X,13HKOUNT FOR K2=,1X,I2)
0012
0013
                       77 READ(5,200, END=88) DATE
CO14
0015
                           WRITE(6,201) DATE
0016
                           READ(5,IN)
0017
                           READ (5, CONST)
0018
                           WRITE (6, 102)
0019
                           DO B I=1.NC
0020
                           WRITE(6,103) DS(I),SN(I),COMC(I),I
0021
                         8 CONTINUE
0022
                           ZONE = (1.00,0.00)
0023
                            ZOONE = (0.D0 .1.D0)
0024
                           ONE=1.DO
0025
                           TW0=2.00
0026
                            TWOC = ZONE + TWO
                           WL=2.997924562D1/FGH
0027
0028
                           PII3=6.2831853072D0/WL
0029
                            PII4=6.28318D0/WLG
                           WRITE (6, CONST)
0030
                           WRITE(6,100)
XOG=WLG/4.DO-DELN
0031
0032
                            TANG=DTAN(PI14+XOG)
0033
0034
                            EG=PII4+DG/TWO
0035
                            YG=(ZODNE+(-C))+(ZONE-ZODNE+(EG+TANG))/((ZONE+EG)-(ZODNE+YANG))
0036
                            DO 10 I=1,NC
                            XOS=XOG-(GN-SN(I))
0037
                            TANS=DTAN(PII4+XOS)
0038
0039
                            THETA=PII4+DS(I)/TWO
                            ES=DSIN(THETA)/DSQRT(TWO-(DCOS(THETA))++2)
0040
0041
                            YT=(ZOONE+(-C))+(ZONE-ZOONE+(ES+TANS))/((ZONE+ES)-(ZOONE+TANS))
0042
                            YS=YT-YG
0043
                            KIM=FAKE(1)
                            K2M=-FAKE(2)
0044
                            K1M=K1M+ONE
0045
0046
                            K1=K1M+C1+K2M
0047
                            K2=K2M
                            KM=DSQRT(K1 ++2+K2++2)
0048
0049
                            KMA=DSQRT((KM-K1)/TWO)+PII3+R
0050
                            KMB=DSQRT((KM+K1)/TWO)*PII3*R
0051
                            KMAC = ZONE + KMA
0052
                            KMBC = ZOONE + KMB
0053
                            GR=KMBC+KMAC
0054
                            D2C=ZONE+16.D0
0055
                            D3C=ZONE+384.00
0056
                            D4C=ZONE+1.8432D4
0057
                            DSC=ZONE*4.DO
0058
                            D6C=ZONE+64.DO
0059
                            D7C=ZONE+2304.D0
0060
                            J11=GR/TWOC
0061
                            J12=GR++3/D2C
0062
                            J13=GR**5/D3C
0063
                            J14=GR**7/D4C
```

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Program 1, continued

```
0064
                         J1=J11+J12+J13+J14
0065
                         JO1=ZONE
0066
                         J02=GR++2/D5C
                         J03=GR++4/D6C
0067
                         J04=GR++6/D7C
0068
                         J0=J01+J02+J03+J04
0069
0070
                         RATIO=(TWOC/GR)+J1/J0
                         K1C=ZDNE+K1
0071
                         K2C=ZDONE+(-K2)
0072
0073
                         KC=K1C+K2C
0074
                         KCOR=KC+RAT IO
                         K1CAL=FUN(1)
0075
                         K2CAL = - FUN(2)
0076
                         ERROR = DSQRT ( (K1M-K1CAL) ++2+(K2M-K2CAL) ++2)
0077
0078
                         DO 400 K=1,4
                         DO 600 J=1,2
0079
                         WE=ONE+STEP (K) +F(J)
0080
0081
                         KOUNT = 0
0082
                    401 K10LD=K1
0083
                         KOUNT = KOUNT +1
                         EROLD = ERROR
0084
                         K1=K1 *WE
0085
                         KM=DSQRT(K1 **2+K2**2)
0086
                         KMA=DSORT((KM-K1)/TWO)*PII3*R
KMB=DSORT((KM+X1)/TWO)*PII3*R
KMAC=ZONE*KMA
0087
0088
0089
                         KMBC = ZOONE + KMB
0090
0091
                         GR=KMBC+KMAC
                         D2C=ZONE+16.D0
0092
                         D3C=ZONE+384.D0
E 600
                         D4C=ZONE+1.8432D4
0094
0095
                         D5C=ZONE+4.D0
0096
                         D6C=ZONE+64.D0
                         D7C=ZONE+2304.D0
0097
                         J11=GR/TWOC
0098
0099
                         J12=GR++3/D2C
0100
                         J13=GR++5/D3C
                         J14=GR++7/D4C
0101
0102
                         J1=J11+J12+J13+J14
0103
                         J01=2 DNE
0104
                         J02=GR++2/D5C
0105
                         J03=GR++4/D6C
0106
                         J04=GR**6/D7C
                         J0=J01+J02+J03+.104
0107
                         RATIO=(TWOC/GF) 4 1 'UO
0108
0109
                         K1C=ZONE*K1
 0110
                         K2C=ZOONE+(-K2)
 0111
                         KC=K1C+K2C
                         KCOR=KC+RATIO
 0112
 0113
                         K1CAL = FUN(1)
 0114
                         K2CAL = - FUN(2)
 0115
                         ERROR = DSQRT ((K1M-K1CAL) **2+(K2M-K2CAL) **2)
0116
                         IF(KOUNT.GT.20) GO TO 601
                         IF(ERROR.LE.EROLD) GO TO 401
 0117
 0118
                         K1=K1OLD
                         ERROR = EROLD
 0119
                     600 CONTINUE
 0120
                         GO TO 602
 0121
 0122
                     601 WRITE(6,104) KOUNT
                     602 DO 700 J=1,2
 0123
                         WE=DNE+STEP(K)+F(J)
 0124
 0125
                         KOUNT = 0
 0126
                     421 K20LD=K2
 0127
                          KOUNT = KOUNT +1
 0128
                          EROLD = ERROR
 0129
                          K2=K2+WE
                          KM=DSQRT(K1++2+K2++2)
 0130
 0131
                          KMA=DSQRT((KM-K1)/TWD)*PII3*R
                          KMB=D5QRT((KM+K1)/TWO)*P113+R
 0132
```

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```
Program 1, continued
```

```
0133
                         GR=KMBC+KMAC
0134
                         D2C=ZONE+16.00
0135
                         D3C=ZONE+384.D0
0136
                         D4C=ZONE+1.8432D4
0137
                         D5C=ZONE+4.D0
0138
                         D6C=ZONE+64.DO
0139
                        D7C=ZDNE+2304.D0
0140
                         J11#GR/TWOC
0141
                         J12=GR**3/D2C
0142
                         J13=GR**5/D3C
0143
                         J14=GR++7/D4C
0144
                         J1=J11+J12+J13+J14
0145
                         J01=ZONE
0146
                         J02=GR++2/D5C
0147
                         J03=GR**4/D6C
0148
                         J04=GR**6/D7C
0149
                         J0=J01+J02+J03+J04
0150
                         RATIO=(TWOC/GR)+J1/JO
0151
                         K1C=ZONE+K1
0152
                         K2C=ZOONE+(-K2)
0153
                         KC=K1C+K2C
0154
                         KCOR=KC+RATIO
0155
                         K1CAL=FUN(1)
0156
                         K2CAL=-FUN(2)
0157
                         ERROR = DSQRT ((K1M-K1CAL) ++2+(K2M-K2CAL) ++2)
                        IF(KOUNT.GT.20) GO TO 701
IF(ERROR.LE.EROLD) GO TO 421
0158
0159
0160
                         K2=K20LD
0161
                        ERROR = EROLD
0162
                    700 CONTINUE
0163
                        GD TO 702
0164
                    701 WRITE(6,105) KOUNT
0165
                    702 IF(ERROR.LE.1.D-4) GO TO 450
0166
                    400 CONTINUE
0167
                    450 SIGMA = SMF + K2
0168
                        WRITE(6,101) CONC(I), K1, K1M, K2, K2M, SIGMA, ERROR, J04, J14
0169
                     10 CONTINUE
                     GO TO 77
88 CALL EXIT
0170
0171
0172
                        END
```

```
Output 3GHZ 21.3 DEG.C.
```

```
DS
            SN
                         CUNC
                                       I
0.0679
           0.3032
                        0.0
0.2009
           0.3159
                       1.1090
0.6445
           0.3835
                       5.0434
                                        3
1.1360
            0.5070
                       10.0760
```

&CONST

DG= .120000000000000000D-01,GN= .47999999999999 ,DELN= .219700000000000000

WT%ACID	K 1	UNCOR, KI	K2	UNCOR. K2	SIGMA MHO	CM ERROR	
0.0	77.45	77.73	12.24	12.34	9.02041	0.240-01	
1.109	71.70	71.84	41.14	41.43	0.06856	0.33D-01	
5.043	40.68	39.82	134.86	135.40	0.22477	0.190-01	
10.076	-12.93	-15.64	231,21	230.75	0.38534		
		***			J04	J14	1
				-0		•	70-09 -0.270-09
				•			
				-0	.110-09 0.1 .640-07 -0.5	7D-07 -0.3	37D-09 0.97D-10 24D-08 0.59D-09 79D-08 -0.12D-07

Program 2 is used for calculating the results for a temperature run on a thin sample (in coax or hollow waveguide) located on a quarter-wavelength spacer. The variations in data with temperature of the empty sample holder with, and without, the spacer are expressed as a power series of temperature change from room temperature. Corrections can then be made for the change in electrical length of the spacer with temperature. Partial notation follows:

DXQC	node width for holder with spacer only, corrected for temperature effects
DAC	node width for empty holder corrected for temperature
ANC	node position for empty holder versus temperature
QNC	node position for holder with spacer only corrected for changes with temperature
DQC	spacer length versus temperature
THC	sample thickness corrected for linear thermal expansion

Program . Thin Sample temp. run

FORTRAN IV G1 RELEASE 2.0

0001	
2) W W 2 WC1 C2.TC6.K3.TANW2.TCW.DOC.DG.TCO.DAC.A5.A6.DXQC,	
3DXQ,AQ,AQQ,DXQCC,QN,AN,TC1,TC2,TC3,ANC,QNC,TC7,TCE,TC9,TXQQ,	
4W2, PII3, U, TA1, DC, DX, SN, COSINE, TXOS, Z11RE, Z11IM, SILLY (2), AZ11,	
5AZ16, A.B. FUN(2), TAHA, TANB, A2, B2, Z14RE, Z14IM, ERROR; .WE, BOLD,	
GSTEP(5)/1.D-2,1.D-3,1.D-4,1.D-5,1.D-6/,F(2)/1.D0,-1.D0/,Z1410D,	
7Z14ROD, EROLD, AOLD, FCC, FAKE(2), RA, AIM, C1, TC6, C2C, C2, KAPPA, TAND, L1	١.
8L2,L3,R,KAPPAC,TANDC.RE,TAM,SIGMA,PUN(2),DS,C1C,D2,D3,AX,WL1	,
O003 COMPLEX*16 ZONE, ZONE, X,Y,Z32,AL102,BE102,G102,Z4,Z10,Z11,Z10, 2Z12SQ,THG2D2,Z14,Z12RE,Z12IM,Z12NEW,Z13,G,H,Z15,Z17,G2D2,K3C,Z14	IR.
3Z14I 0D04 DIMENSION DS(30),SN(30),D2(30),D3(30),DATE(39),AX(30),T(30)	
0004 DIMENSION DS(30), SN(30), D2(30), D3(30), DATE(39), AX(30), I(30)	
0005 EQUIVALENCE (SILLY(1), Z4), (FAKE(1), Z15), (FUN(1), Z14),	
2(PUN(1),Z12SQ) 0006 NAMELIST/CONST/DA.DXQ.DQ.FC.LW.DT.TCW.TCQ.A5.A6, 4Q.AQQ.TC1,TC2.	۲a.
0006 NAMELIST/CONST/DA.DXQ.DQ.FC.LW.DI.ICW.TCQ.AB.AB.AB.AQ.AQQ.TCT.TCZ.	,
2TC3.TC7.TCB.TC9,TCD.TC6,C1,C2,D,AN,QN/IN/DS,SN,1,D2,D3,AX,	
3NX/OUT/A,B,AZ11,AZ16,Z125Q,Z11,Z16	
0007 200 FORMAT(1X,39A2)	
COOR 20. FORMAT(1H0, 20X, 39A2)	
0009 220 FORMAT (1H0,5X,2HDS,8X,2HSN,6X,2HD2,7X,2HD3,7X,2H X,8X,	
24HTEMP,6X,1HI)	
0010 230 FDRMAT(2X,F8.4,1X,F8.4,2X,F7.4,2X,F6.4,2X,F8.5,2X,F8.2,2X,I2)	
0011 100 FORMAT(1H0,5x,2HNS,6x,2HDS,4x,7HD,CORR.,4x,2HFC,6x,1HB,6x,2HK1,	
29X,2HK2,9X,3HTAN,15X,6HZ4/Z14//)	
0012 300 FORMAT(2X, F7.4, 2X, F7.4, 1X, F7.4, 1X, F7.4, 1X, F7.4, 1X, F7.4, 3X, F9.6,	
23X, F9.6.3X, E13.6.2X, E13.6)	
0013 301 FORMAT(10X, 6HTEMP.=, F7.1, 1X, 6HDEG.C., 4X, 6HSIGMA=, E11.4.6HMHO/CM	•
25X,19HSAMPLE HOLDER DIA.=,F8.5)	
0014 77 READ(5,200, END=88) DAYE	
0015 WRITE(8,201) DATE	
0016 READ(5.CONST)	
0017 READ(5.IN)	
0018 WRITE(6,220)	
0019 WRITE(6,230)(DS(1),SN(1),D2(I),D3(I),AX(I),T(I),I,I=1,NX)	
0020 WRITE(6,CONST)	
0021 WRITE(6,100)	
0022 ZNNE=(1.D0.0.D0)	
0023 ZDGNE=(0.D0,1.D0)	
0024 ONE=1.D0	

```
Program 2, continued
                        TW0=2.00
0025
                        P11=3.1415926536D0
 0026
 0027
                        P112=TWO+P11
                        W=ONE+FC
002B
 0029
                        WIRW
                        TANW1 = DA/(DT+W1)
 3030
                        WL1=LW
 0031
                        LW02=LW++2/W
 0032
                        DO 10 I=1,NX
 0033
                        THC=D*(ONE+(T(I)-TO)*TCD)
 0034
                        IF(FC.GT.O.DO) GO TO 33
 0035
                        WL2=LW
 0036
                        WC2=1.D30
 0037
 003B
                        GO TO 35
                     33 WC1=3.412586D0+1.27DC+C2
 0039
 0040
                        WC2=WC1*(ONE+TC6+(T(I)-T0))
 0041
                        WL2=DSQRT(LW02*WC2++2/(WC2++2-LW02))
 0042
                     35 K3=WL2/(PII2+THC)
 0043
                        W2=(WL2/WC2) == 2+ONE
                        TANW2 = TANW1 +DSQRT(ONE+TCW+(T(I)-T0))+W1/W2
 0044
 0045
                        DQC=DQ+(ONE+TCQ+(T(1)-TO))
 0046
                        DAC=DA+(ONE+A5*(T(T)-T0)+A6*(T(I)-T0)++2)
                        DXQC=DXQ+(ONE+AQ+(T(I)-T0)+AQQ+(T(I)-T0)++2)
 0047
 0048
                        DXQCC=DXQC-DAC-(QN-AN) +W1+TANW1+DQC+W2+TANW2
 0049
                        ANC=AN-TC1+(T(1)-T0)-TC2+(T(1)-T0)++TC3
 0050
                        QNC=QN-TC7* (T(I)-T0)-TCB*(T(I)-T0)**TC9
                        TXOQ=DTAN(PI12+((QNC-ANC)/WL1-DQC/WL2))
 0051
 0052
                        X=ZONE+(DXQCC+PII/WL2)
 0053
                         Y = ZOONE + ( -T XOQ)
 0054
                        ZB2=(X+Y)/(ZONE+X+Y)
 0055
                        PII3=PII2/WL2
 0056
                         U=W2-0NE
 0057
                        TA1=DSQRT(ONE+(TANW2/(ONE-U/(1.00054D0+W2)))++2)
 0058
                        AL1D2=ZONE+ (PII3+DSQRT(5.D-1+(1.00054+W2-U)+(TA1-ONE))+THC)
                         BE1D2 = ZGONE - (PII3 + DSQRT (5.D-1+(1.00054 + W2-U)+(YA1+ONE))+THC)
 0059
 0060
                        G1D2=AL1D2+BE1D2
 0061
                        DC=DQC+THC
                        DX=DS(I)-DXQC-(SN(I)-QN)+W1+TANW1+DC+W2+TANW2
 0062
 0063
                         COSINE=DCDS (PII+DX/WL2) *+2
 0064
                         X=DSIN(PII+DX/WL2)/DSQRT(AX(I)-COSINE)
 0065
                         TXOS = DTAN(PII2*((SN(I)-ANC)/WL1-DC/WL2))
                         Y=ZDONE + ( -T XOS)
 0066
                         Z4=(X+Y)/(ZONE+X+Y)
 0067
                         210=200NE/K3
 0068
                         Z11=Z10/24
 0069
 0070
                         Z11RE=SILLY(1)
 0071
                         Z11IM=SILLY(2)
 0072
                         Z16=(1.00/3.00)*Z11**2
 0075
                         Z12SQ = CDSQRT(Z11+Z16)
 0074
                         AZ11=CDABS(Z11)
 0075
                         AZ16=CDABS(Z16)
                         A=PUN (1)
 0076
                         B=PUN (2)
 0077
 0078
                         IF(0.D0.LT.B) GO TO 160
 0079
                         WRITE (6, OUT)
 0080
                         B=1.00
 0081
                    160 TAHA=DTANH(A)
 0082
                         TANB=DTAN(B)
 0083
                         A2=TAHA+(UNE+TANB++2)/(ONE+TAHA++2+TANB++2)
 0084
                         B2=TANB+ (ONE-TAHA++2)/(ONE+TAHA++2+TANB++2)
                         THG2D2=ZDNE +A2+ZOONE+B2
 0085
 0086
                         G2D2=ZONE*A+ZCONE*B
 0087
                         Z14=(Z0NE+G1D2+THG2D2/(Z82+G2D2))/(Z0NE/Z82+G2D2+THG2D2/G1D2)
                         Z14RE = FUN(1)
 CORR
 0089
                         Z14IM=FUN(2)
 0090
                         ERROR 1-DSQRT((Z14RE-Z11RE)++2+(Z14IM-Z11IM)++2)
```

.!

```
Program 2, continued
```

```
DO 400 K=1.5
2092
                       TAHA=UTANH(A)
0093
                       DO 600 J=1,2
0094
                       WE=ONE+STEP(K)+F(J)
0095
                   401 BOLD # B
0096
                        21410D#2141M
0097
                        Z14R0D=214RE
0098
                        EROLD = ERROR 1
0099
                        B=B+WE
0100
                        TANB=DTAN(B)
                        A2=TAHA+(ONE+TANB##2)/(ONE+TAHA##2+TANB##2)
0101
0102
                        B2=TANB+(ONE-TAHA++2)/(ONE+TAHA++2+TANB++2)
0103
                        THG2D2 = ZONE +A2+ZOONE + B2
0104
                        G2D2=ZONE=A+ZOONE+B
0105
                        Z14=(Z0NE+G102+THG2D2/(Z82+G2D2))/(Z0NE/Z82+G2D2+THG2D2/G1D2)
0106
                        Z14RE = FUN(1)
0107
                        Z14IM=FUN(2)
0108
                        ERROR1=DSQRT((Z14RE-Z11RE)++2+(Z14IM-Z111M)++2)
0109
                        IF (ERROR1. LE. EROLD) GO TO 401
0110
                        Z141M=Z1410D
0111
                        Z14RE=Z14ROD
0112
                        B=BOLD
0115
                        ERROR 1 = EROLD
                   600 CONTINUE
0113
0115
                        TANB=DTAN(B)
0116
                        DO 700 J=1.2
                        WE = ONE+STEP (K) +F(J)
0117
0118
                   402 AOLD=A
0119
                        Z14ROD=Z14RE
0120
                        Z14100=Z141M
0121
                        EROLD = ERROR 1
0122
                        A=A-WE
0123
                        TAHA=DTANH(A)
0124
                        A2=TAHA+(ONE+TANB++2)/(ONE+TAHA++2+TANB++2)
0125
                        B2=TANB+(ONE-TAHA++2)/(ONE+TAHA++2+TANB++2)
                        THG2D2=70NE +A2+Z00NE+B2
0125
0127
                        G2D2=ZONE+A+ZOONE+B
0128
                        Z14=(ZCNE+G1D2+THG2D2/(ZB2+G2D2))/(ZONE/ZB2+G2D2+THG2D2/G1D2)
0129
                        214RE = FUN(1)
0130
                        2141M=FUN(2)
0131
                        ERROR1 = DSQRT((Z14RE-Z11RE) ++2+(Z14IM-Z11IM) ++2)
                        IF(ERROR). LE. EROLD) GO TO 402
0132
0133
                        Z14RE = Z14ROD
                        Z:41M=Z1410D
0134
0135
                        A=ADLD
0136
                        ERROR 1 . EROLD
0137
                    700 CONTINUE
0138
                        IF(ERROR1.LE.1.D-6) GO TO 450
0134
                    400 CONTINUE
0140
                    450 Z12RE=ZONE+A
0141
                        Z121M = Z00NE +B
                        Z12NEW=(Z12RE+Z12IM)++2
0142
0143
                        K3C=K3+ZONE
0144
                        Z13=-Z12NEW+K3C++2
0145
                        FCC=U
0146
                        G=ZONE + FCC
0147
                        H=ZONE=W2
0148
                        215=(G+Z13)/H
0149
                        Z14R=ZONE+Z14RE
0150
                        Z141=700NE + Z14IM
0151
                        Z14=Z14R+Z14I
0152
                        Z17=Z4/Z14
0153
                        RAMFAKE(1)
                        AIM=-FAKE(2)
0154
0155
                        C1C=C1+(ONE+(T(I)-T0)+TC6)
0156
                        C2C=C2+(ONE+(T(1)-T0)+TC6)
0157
                        KAPPA * FARE(1)
0158
                        TAND=AIM/RA
0159
                        IF(FC.GT.0.00) GO TO 210
```

```
Program 2, continued
                         L1=DLOG10(D2(1)/C1C)+DLOG10(C2C/D3(1))
   0161
                         L2=DL0G10(D3(1)/D2(1))
   0162
                         L3=DL0G10(C2C/C1C)
   0163
                         R=DNE-L1+KAPPA+(ONE+TAND++2)/L3
   0164
                         KAPPAC=R+KAPPA/((L3/L2)-TWO+L1+KAPPA/L2+(ONE-R)+L1+KAPPA/L2)
   0165
                         TANDC = TAND / R
   0166
                         RE=KAPPAC
   0167
                         TAM=TANDC-TANW2
   0168
                         AIM=RE+TAM
   0169
                         GO TO 15
   0170
                     210 RE*RA+8368.D-4*(RA**2-RA)*(C2C-D3(1))/C2C
   0171
                      18 TAM=AIM/RE-TANW2+(4.20-1+W2/RA)/(4.20-1+W2)
   0172
                         AIM= DF * TAM
   0173
                      15 WRITE(6,300) ANC, DX, THC, FCC, B, RE, AIM, TAM, Z17
   0174
                         SIGMA=1.6669198D-2+AIM/DSQRT(LW02)
   0175
                         WRITE(6,301) T(1),SIGMA,C2C
   0176
                      10 CONTINUE
   0177
                         GD TO 77
   0178
                      88 CALL EXIT
   0179
                         END
   Output .
                      RAYTHEON POLYIMIDE LAMINATE (OAK) TEMP. RUN
                                                                    8-3-79
       DS
                 SN
                         C2
                                  03
                                                     TEMP
                                                               ĭ
     0.0233
              5.4206
                       0.0
                               0.9948
                                        2,00000
                                                    24.00
              5.3965
                               0.9951
     0.0263
                       0 0
                                        2.00000
                                                    52.00
                                                            2
     0.0251
              3.3842
                       0.0
                               0.9953
                                        2.00000
                                                    77.00
                                                            3
     0.0280
              5.3681
                       0.0
                               0.9956
                                        2.00000
                                                   100.00
  &CONST
  DA= .60000000000000012D-02,DXQ=
                                     .71999999999999990D-02,
    5.9926999999999999
                           .DT= 21.000000000000000
     .4000000000000000019D-03.A6=
                                 . 0
     .4827599999999999993D-03,TC2= .3533000000000000D-08.
     .62090000000000000001D-04.TC8= -.58519000000000023D-09,
     .194299999999999986D-04,C1= .37450000000000000
                           .QN= 5.9591000000000006
    6.1597999999999999
                                                    ,FC= 1.90060000000000007
                        DQ= 1.28760000000000008
                                                                                 . LW =
                          .40000000000000000BD-02,TCQ= .54000000000000005D-06,A5=
                    TCW=
                    TC1=
                                                                               .TC7×
                                                         .999999999999997D-05,TC6=
                     TC9= 3.0000000000000000
                                                  .TCD=
                                                    .66500000000000036D-01,AN=
                    C2= 1.00279999999999991
  NS
          DS
                D, CORR.
                           FC
                                   В
                                          K1
                                                     K2
        0.0166 0.0665 1.9025 0.2238 4.2987
6.1598
                                                  0.059233
               24.0 DEG.C.
                              SIGMA= 0.2806D-03MHO/CM
      TEMP.=
        0.0196 0.0665 1.8965 0.2286 4.4583
6.1463
                                                 0.072154
      TEMP.=
               52.0 DEG.C.
                              51GMA= 0.3419D-03MH0/CM
        0.0194 0.0665 1.8912 0.2306 4.5282
6.1341
                                                  0.071714
                              SIGMA = 0.3397D-03MH0/CM
      TEMP.=
              77.0 DEG.C.
6.1229
        0.0213 0.0666 1.8863 0.2336 4.6312
                                                  0.080035
                              SIGMA= 0.3792D-03MHO/CM
      TEMP. = 100.0 DEG.C.
                                               TAN
                                                                 Z4/Z14
                                             0.013779
                                                         0.100000D+01
                                                                        0.166215D-07
                                         SAMPLE HOLDER DIA. = 1.00280
                                             0.016187
                                                         0.9999990+00
                                                                       -0.248313D-08
                                         SAMPLE HOLDER DIA .- 1.00335
                                             0.015837
                                                         0.100000D+01
                                                                        0.8043820-09
                                         SAMPLE HOLDER DIA. = 1.00383
                                             0.017282
                                                         0.100000D+01
                                                                        0.4023490-08
                                         SAMPLE HOLDER DIA. = 1.00428
```

Program 3 is the latest version for calculating a temperature run for a sample at the bottom of the sample holder. It includes a correction for the fact that a node shift in the hot zone of hollow waveguide does not result in an equal shift in the cold slotted section because the guide wavelengths are different in the two zones. The changes appear in statements 43-47, and 174 in the following program.

Program 3 Shorted Line Temperature Run

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```
INTEGER+4 1.8,K,N,NX,KOUNT,COUNT
0001
                        REAL+8 K3,Y,XE,AN,SN,LW,DX,DS,DA,X,A,B,A2,B2,Z14RE,Z14IM,TWO.
0002
                       2BOLD, Z14IOD, Z14ROD, ERROR1, EROLD, AOLD, AIM, RE, TAM, Z11RE, Z11IM, WE.
                       9KAPPA, KAPPAC, L1, L2, L3, R, TAND, TANDC, D2, D, D3, SNC, TC1, T, T0, TC2, TC3,
                       3COSINE, FC.W.ZM, Y1, TAHA, TANB, PII, PII2, ZRC, ONE, STEP(22)/1.50-2.
                       41.2D-2
                       41.D-2,7.D-3,5.D-3,2.D-3,1.D-3,5.D-4,2.D-4,1.D-4,5.D-5,2.D-5,
                       51.D-5
                       55.D-6,2.D-6,1.D-6,1.D-7,1.D-8,1.D-9,1.D-10,1.D-11,1.D-12/,ND8.
                       GF(2)/1.D0,-1.D0/,SDLD,RA,TANW,DC,DD0,DD,TC4,TC5,WC1,WC2,TC6,LW02,
                       7WL2,DDA,A5,A6,C1,C2.C1C,C2C,FCC,SIGMA,AX,TCD
                         COMPLEX+16 Z1, Z2, Z3, Z9, Z10, Z11, Z12, Z13, Z14R, Z14I, Z16, K3C,
0003
                        2214, Z12NEW, Z12RE, Z12IM, Z12SQ, G, H, Z15, Z2A, ZONE, ZOONE
0004
                         REAL+8 SILLY(2), FAKE(2)
0005
                         EQUIVALENCE (SILLY(1), Z11), (FAKE(1), Z15)
                       DIMENSION DS(30), SN(30), D(30), D2(30), D3(30), N(30), DATE(39), 2T(30), DD(30), AX(30), SIGMA(30), C2C(30)
0006
                         NAMELIST/IN/DS.SN.N.NX.D.D2.D3.T.DD.AX/CONST/DA.AN.FC.LW.TANW.
0007
                        2TC2, TC3, T0, DD0, TC4, TC5, A5, A6, C1, C2, TC6, TC1, TCD
8000
                    200 FOR'AAT(1X,39A2)
                    201 FORMA (11H0, 20X, 39A2)
220 FORMAT(11.2, 5X, 2HDS, 8X, 2HSN, 6X, 1HD, 7X, 2HD2, 7X, 2HD3, 6X, 1HN,
0009
0010
                        20X,2HDD,4X,11HTEMP.DEG.C.)
                    230 FORMAT(2X,F8.4,1X,F8.4,2X,F7.4,2X,F6.4,2X,F8.5,2X,I2,2X,F8.4,
0011
                        22X,F8.2)
                     100 FORMAT(1H0,5X,2HN5,6X,2HD5,4X,7HD,CORR.,4X,2HFC,6X,1HB,6X,2HK1,
0012
                        29X,2hK2,9X,3HTAN,15X,7HZ11/614//)
                    300 FORMAT(2X, F7.4, 2X, F7.4, 1X, F7.4, 1X, F7.4, 1X, F7.4, 1X, F7.4, 3X, F9.6,
0013
                        23X, F9.6, 3X, E13.6, 2X, E13.6)
0014
                     301 FORMAT(SK, SHOEG.C. 4X, 8HSIGMA IN, 1X, 6HMHO/CM, 1X,
                        220HSAMPLE HOLDER DIA."
                     302 FORMAT (10X, P7.1, 4X, E11.4, 10X, F8.5)
0015
                     77 PEAD(5,200, END=GB) DATE
0016
0017
                         WRITE(6,201) DATE
0018
                         READ(5, IN)
                         REAU(5,CONST)
0019
0020
                         WRITE (6, 220)
                         WRITE(6,230)/DS(I),SN(I),D(I),D2(I),D3(I),N(I),DD(I),T(I),I=1,NX)
0021
0022
                         WRITE (6, CONST)
0023
                         WRITE (6, 100)
0024
                         ZONE=(1.00,0.00)
0025
                         ZOONE = (0.D0,1.D0)
0026
                         ONE = 1 . DO
0027
                         TW0=2.00
                         PI1=3.1415926536D0
0028
0029
                         PII2=PII+TWO
0030
                         ZRO=0.DO
0031
                         DO 10 I=1,NX
                         IF(DD(1).EQ.DD0) GO TO 22
0032
                         DC=D(1)+(DDO-DD(1))+2.54DO+TC4+(T(1)-TO)+TC5+(T(1)-TO)+*2
0033
0034
                         GO TO 23
0035
                      22 DC=D(I)*(ONE+(T(I)-T0)*TCD)
                      23 SNC*SN(I)+(TC1*(T(I)-T0)+TC2*(T(I)-T0)**TC3)
9500
```

```
Program 3, continued
0037
                       W=ONE+FC
0038
                        LW02=LW++2/W
0039
                        IF(FC.GT.0.D0) G0 TO 33
0040
                        WL2≖LW
0041
                        WC2=1.D30
0042
                        GD TO 35
                     33 WC1=3.412586D0+1.27D0+C2
0043
0044
                        WC2=WC1+(ONE+TC6+(T(I)-TO))
0045
                        WL2=DSGRT(LW02+WC2++2/(WC2++2-LW02))
                     35 K3=WL2/(P112+DC)
0046
0047
                        Y=PII2+((SNC-AN)/LW-DC/WL2)
0048
                        DDA=DA=(ONE+A5+(T(I)-T0)+A6+(T(I)-T0)++2)
0049
                        DX=DS(I)-DDA
                        1F(DX.LE.ZRO) GO TO 10
0050
                        CUSINE=DCOS (PII+DX/LW)++2
0051
                        X=DSIN(PII+DX/LW)/DSQRT(AX(I)-COSINE)
0052
0053
                        Y1=DTAN(Y)
0054
                        Z1=Z00NE=Y1
0055
                        Z2A=ZONE+X
0056
                        72=72A-21
                        Z3=Z0NE-Z2A+Z1
0057
005B
                        Z9=Z2/Z3
0059
                        Z10=Z00NE+(~K3)
0060
                        Z11=Z10+Z9
0061
                        Z11RE=SILLY(1)
0062
                        Z11IM=SILLY(2)
0033
                        ZM=DSQRT(211RE**2+Z11IM**2)
0064
                        1F(N(1) .EQ. 1) GO TO 141
0065
                        IF(N(I) .GE. 2) GO TO 142
0066
                    141 IF(ZM.LE.ONE.AND.Z11RE.GE.ZRD) GO TO 150
0067
                        IF(ZM.LE.ONE.AND.Z11RE.LY.ZRO) GO TO 151
                        IF(ZM.GT.ONE.AND.Z11RE.GE.ZRO) GO TO 152
IF(ZM.GT.ONE.AND.Z11RE.LT.ZRO) GO TO 153
0068
0069
                    142 IF(ZM.LE.ONE.AND.ZITRE.GE.ZRO) GO TO 170
0070
2071
                        IF(ZM.LE.ONE.AND.Z11RE.LT.ZPD) GO TO 171
0072
                        IF(ZM.GT.ONE.AND.Z11RE.GE.ZRO) GO TO 172
0073
                        IF(ZM.GT.ONE.AND.Z11RE.LT.ZRO) GO TO 173
0074
                    150 B=ONE
0075
                        A=42.0-1 + DX/LW
                        GD TO 160
0076
0077
                    151 B=22'. D-1
007B
                        A=2.D0*DX/LW
0079
                        GD TD 160
0080
                    152 B=ONE
                        A=6.D0.DX/LW
0081
0082
                        GO TO 160
                    153 B=18.D-1
0083
0084
                        A=DX/LW
0085
                        GD TO 160
0036
                    170 ND8=N(1)
0007
                        B=(ND8-ONE)+PII+7854.D-4
00BB
                        A=4.00+DX/LW
                        GO TO 160
0089
0090
                    171 ND8=N(I)
0091
                        B=N08 * P11-7854.0-4
0092
                        A=4.D0*DX/LW
0093
                        GO TO 160
0094
                    172 ND8=N(I)
0095
                        B=(2.D0*ND8-1.D0) *15708.D-4-2.D-1/ND6
0096
                        A=DX/LW
0097
                        GO TO 160
0098
                    173 NDB=N(I)
0099
                        B=(2.D0+ND8-1.D0)+15708.D-4+2.D-1/ND8
0100
                         A=DX/LW
```

160 TAHA DTANH(A)
TANB DTAN(B)

0101

0102

0103

0105

0106

A2=TAHA+(ONE+TANB++2)/(ONE+TAHA++2+TANB++2)

B2=TANB+(ONE-TAHA++2)/(ONE+TAHA++2+TANB++2)

Z14RE=(A+A2+B+B2)/(A++2+B++2)

Z14IM=(A+B2-B+A2)/(A+=2+B++2)

```
Program 3, continued
0107
                        ERROR1=DSQRT((Z14RE-Z11RE)++2+(Z14IM-Z11IM)++2)
0108
                        COUNT = 0
0109
                    440 COUNT = COUNT +1
                        DO 400 K=1.22
0110
                        SOLD STEP(K)
0111
0112
                        1 AHA = DTANH(A)
0113
                        DO 600 J=1.2
0114
                    420 WE=ONE+STEP(K)=F(J)
0115
                        KOUNT = 0
                    401 KOUNT = KOUNT +1
0116
                        IF(KOUNT.GT.10.AND.STEP(K).LE.1.D-3) GO TO 411
0117
0118
                        GD TO 425
                    411 STEP(K)=STEP(K)+1C.DO
0119
0120
                        GO TO 420
0121
                    425 BOLD=B
0122
                        214100=Z141M
0123
                        Z14RDD=Z14RE
                        EROLD = ERROR 1
0124
                        B=B+WE
0125
                        TANB DTAN(B)
0126
0127
                        A2=TAHA+(ONE+TANB++2)/(ONE+TAHA++2+TANB++2)
0128
                        B2=TANE*(ONE-TAHA**2)/(ONE+TAHA**2*TANB**2)
                        Z14RE = (A+A2+B+B2)/(A++2+B++2)
0129
                        Z141M=(A+B2-B+A2)/(A++2+B++2)
0130
                        ERROR1=DSQRT((Z14RE-Z11RE)++2+(Z14IM-Z11IM)++2)
0131
0132
                        IF(ERROR1, LE. EROLD) GO TO 401
0133
                        Z14IM=Z14IDD
0134
                        Z14RE = Z14ROD
0135
                        B=BOLD
0136
                        ERROR1 = EROLD
 0137
                        STEP(K)=SOLD
                    600 CONTINUE
013B
 0139
                        TANB=DTAN(B)
 0140
                        DO 700 J=1,2
 0141
                    421 WE=ONE+STEP(K)+F(J)
 0142
0143
                    402 KOUNT = KOUNT +1
 0144
                        IF(KOUNT.GT.10.AND.STEP(K).LE.1.D-3) GO TO 412
0145
                        GC TG 428
 0146
                    412 STEP(K) = STEP(K) +10.00
 0147
                    GO TO 421
428 ADLD=A
 0148
 0149
                        714RQD=Z14RE
 0150
                        71410D=Z141M
                        ERGLD=ERROR 1
 0151
 0152
                        A=A+WE
                        TAHA = DTANH(A)
 0153
 0154
                        A2=TAHA+(ONE+TANB++2)/(ONE+TAHA++2+TANB++2)
 0155
                        B2=TANB+(ONE-TAHA++2)/(ONE+TAHA++2+TANB++2)
 0156
                        Z14RE = (A*A2+B+82)/(A*+2+B+*2)
 0157
                        Z14IM=(A+32-B+A2)/(A++2+B++2)
 0158
                        ERROR 1 = DSQRT((Z14RE-Z11RE)++2+(Z14IM-Z11IM)++2)
 0159
                         IF(ERROR1.LE.EROLD) GO TO 402
 0160
                        Z14RE=Z14ROD
 0161
                         214IM=214IOD
 0162
                         A=AOLD
 0163
                        ERROR 1 = EROLD
 0164
                        STEP(K)=SOLD
 0165
                    700 CONTINUE
 0166
                         IF(ERROR1.LE.1.D~7) GO TO 450
 0167
                    400 CONTINUE
 0168
                         IF(ERROR1.GT.1.D-7.AND.COUNT.LE.2) GO TO 440
 0169
                     450 Z12RE=ZONE+A
                         Z12IM=ZDONE +B
 0170
 0171
                         Z12NEW=(Z12RE+Z12IM)++2
 0172
                         K3C=K3+ZONE
 0173
                         Z13=-Z12NEW#K3C##2
                         FCC=WL2*+2/WC2++2
 0174
                         W=ONE+FCC
 0175
                         G=ZONE + FCC
```

0176

```
Program 3, continued
```

```
H=ZONE+W
                       Z15=(G+Z13)/H
0178
                       Z14R = ZONE + Z 14RE
0179
                       Z141 = ZOONE + Z141M
0180
                       214=214R+214I
0181
                       216=211/214
0182
                       RA=FAKE(1)
0183
                       AIM=-FAKE(2)
0184
                       C1C=C1+(ONE+(T(I)-T0)+TC6)
0185
                       C2C(I)=C2*(ONE+(T(I)-T0)*TC6)
9186
                        KAPPA=FAKE(1)
0:87
                        TAND=AIM/RA
0188
                        IF(FC.GT.0.DO) GO TO 210
0189
                        L1=DL0G10(D2(1)/C1C)+DL0G10(C2C(1)/D3(1))
0190
0191
                        L2=DLOG10(D3(I)/D2(I))
0192
                        L3=DL0G10(C2C(I)/C1C)
                        R=ONE-L1*KAPPA*(ONE+TAND++2)/L3
0193
                        KAPPAC=R+KAPPA/((L3/L2)-TWO+L1+KAPPA/L2+(ONE-R)+L1+KAPPA/L2)
0194
                        TANDC = TAND/R
0195
0196
                        RE=KAPPAC
                        TAMETANDC-TANW+DDA/DA
0197
                        AIM=RE*TAM
0198
                        GO TO 15
0199
                   210 RE=RA+8368. D-4*(RA**2-RA)*(C2C(I)-D3(I))/C2C(I)
0200
                     18 TAM=AIM/RE-TANW=DDA+(4.2D-1+W/RA)/((4.2D-1+W)+DA)
0201
0202
                        AIM=RE + TAM
0203
                    15 WRITE(6.300) SNC, DX, DC, FCC, B, RE, AIM, TAM, Z16
                        SIGMA(I)=1.66691980-2#AIM/DSQRT(LW02)
0204
                     10 CONTINUE
0205
                        WRITE (6,301)
0206
0207
                        DO 11 I=1,NX
                        WRITE(6,302) T(1),SIGMA(1),C2C(1)
0208
                     11 CONTINUE
0209
                        GO TO 77
0210
0211
                     88 CALL EXIT
                        END
0212
```

In the latter part of this report period we have investigated the possibility of using derivatives in one shorted line (also corresponding relations in the open circuited line) calculations for finding a and b in the expression

$$tanh (a + jb) / (a + jb) = C + jD$$

when C and D are known. In principle the use of derivatives to extrapolate to the solution could provide faster, more efficient programs than the blind stepping method we have used. In practice we found that the damping required (in a general use program) because of large changes in values of the derivatives resulted in little or no improvement.

If approximately correct initial values of a and b are obtained from charts (or in the case of thin samples at the quarter wave plane, from algebraic expressions) iteration using derivatives is useful, as in our programs for the HP9810A calculator. These are available on request.

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DIELECTRIC PARAMETERS

Dielectric parameters in this series of reports have the variables in one of the following notations:

- κ^{\bullet} , $\epsilon^{\bullet}/\epsilon_{0}$, K, Kl, dielectric constant relative to vacuum
- $\kappa^{\prime\prime}\text{, }\epsilon^{\prime\prime}/\epsilon_{0}\text{, }\text{K2, dielectric loss factor relative to vacuum}$
- tan δ , tan δ_d , TAN DELTA, D.F., dielectric loss tangent (dissipation-factor)
- $\kappa_{m}^{t},~\mu^{t}/\mu_{0},$ magnetic pearmeability relative to vacuum
- $\kappa_m^{\prime\prime},~\mu^{\prime\prime}/\mu_0,$ magnetic loss factor relative to vacuum
- tan δ_{m} , magnetic loss tangent
- o, a.c. volume conductivity in mho/cm
- ρ , a.c. volume resistivity in ohm-cm

with the last of the second of

MATERIALS INDEX

I. Inorganic Compounds

Aluminum nitrides General Electric/RSD Measurements made under AMMRC contract DAAG46-79-C-0096, reference AMMRC report AMMRC-TR81-45 (March 1982)

to deposit:	GHz,E par ion plane	allel	Hot-pressed	(HP-21)	2.64 gm/cc(81%)
Toc	K	tan o	т ^о с	ĸ	tan δ
30 96 205 300 401 518 589 672 723 800	7.47 7.56 7.68 7.83 7.98 8.21 8.36 8.59 8.74	.0020 .0019 .0026 .0122 .0225 .0606 .110 .181 .248	27.5 136 222 311 408 507 607 708 738 800	5.963 6.038 6.090 6.144 6.202 6.285 6.380 6.457 6.492 6.549	.00216 .00243 .00275 .00239 .00234 .00276 .00320 .00372

Aluminum oxide

Single crystal, sapphire

Unknown

E	T	to	optic	axis,	8.5	GHz
---	---	----	-------	-------	-----	-----

	κ	$tan \delta$
Sample 1	9.42	$.00006 \pm .00004$
2	9.38	<.00002

Ceramic, Wesgo 4078 8.5 GHz, 24°C

Western Gold & Pt.

κ tan δ
9.31 .00034

Aluminum	oxynitride	crystal			Αl	MMRC	
T°C	Freq., Hz	10 ²	103	104	105	10 ⁶	107
25	κ' tan δ σ	8.56 .0015 7.1E-13	8.56 .0011	8.56 .0006	8.56 .0005	8.56 .0005	8.56 .0004
150	κ' tan δ σ	8.62 .0033 1.6E-12	8.60 .0037	8.60 .0024	8.60 .0018	8.60 .0010	8.60 .0006
300	κ¹ tan δ σ	8.97 .0270 1.343E-11	8.79 .0108	8.72 .0044	8.65 .0029	8.64 .0026	8.64 .0021
400	κ' tan δ σ	10.0 .0709 3.94E-11	9.40 .0495	9.13 .0229	8.95 .0078	8.76 .0037	8.72 .0031
500	κ' tan δ σ	14.0 1.014 7.89E-10	11.7 .212 1.38E-9 -1	9.92 .0941 8-	9.18 .0370	8.95 .0136	8.87 .0070

Beryllium oxide

Ceramics

4185	Ceradyne	K150			Unknown
23°C, 8.5 C Density = 2	SHz 3	23 ⁰ C, 8.5 GHz			
-	_	Sample	Density (g/cm ³)	κ	tan δ
K' = 0.00;	$\tan \delta = .00030$	1 2	2.8 91 2.8 8 2	6.715 6.688	.00037

Boron nitride

Cubic, CVD Specimen No. 1025(3) 24°C, 24 GHz

General Electric/RSD measured under AMMRC Contract No. DAAG46-79-C-0047; reference AMMRC TR79-45(August, 1979)

 $\kappa' = 7.01$; tan $\delta = .0048$

Hot-pressed, 8.5 GHz, 24°C

Grade HP		Carbo	orundum	Grade HBC		Uni	Union Carbide		
	Sample	Density (g/cm ³)	κ	tan δ	Sample	Density (g/cm ³)	К	tan δ	
	1	1.895	4.28	.00078	1	1.943	4.10	.00015	
	2	1.879	4.27	.00078	2	1.944	4.08	.00013	

Woven fiber

BN-3	DX 59-1-1.74			14 GHz		Ford Aerospace
	24°C			Face 1,	rotation 0°	
Face	Rotation, °	κ	tan δ	т°С	κ	tan δ
1	0	3.775	.00111	200	3.796	.00105
	90	3.683	.00047	400	3.797	.00114
2	0	3.706	.00066	600	3.805	.00092
	90	3.720	.00148	800	3.818	.00135

Cordierite ceramics

Brunswick 2	, 8.5 GH	z				Brunswick
	Against	short			λ/4 awa	y Density
Sample	Face	κ	tan δ	κ	tan δ	(g/cm ³)
1	1	4.735	.00050			2.4472
	2	4.729	.00047			
2	1	4.730	.00050	4.69	.00047	2.5521
	2	4.722	.00047			
3	1	4.717	.00051			2.4372
	2	4.711	.00056			,

Cordierite ceramics (cont.)

Brunswick 2 (1+2+3) stacked Silver paint + silver foil

Brunswick 2-2

Resonan	t-cavity met		Star	ding-wave	method	
т ^о с	κ	tan δ		T ^O C	K	tan 6
25 81	4.7237 4.7410	.00050		23	4.729	.00052
103	4.7484	.00054		100 200	4.754 4.790	.00054 .00062
133.5 162	4.7585 4.7664	.00057 .00058		300 400	4.829 4.863	.00137 .00283
200	4.781	.00066		500	4.890	.00283
232 261	4.7936 4.806	.00081		600 700	4.935 4.980	.0115 .0228
372 409	4.8464 4.8606	.0023		900	5.09	.080
418	4.865	.0033 .0035	$\frac{\Delta K/K}{\Delta T}$ at	300 ⁰ C ≖	4.8205-4. 4.7237 x	$\frac{7237}{375} = 7.45E-5$;
457 500	4.886 4.937	.0046 .0061				275
	,,,,,,,	10001	$\frac{\Delta K/K}{\Delta T}$ at	900°C -	8.70E-5	

Coor CD1	•					Coors
	Agains	t short	short			
Sample	Face	K	tan δ	κ	tan δ	Density (g/cm ³)
1	1 2	4.858 4.859	.00133 .00129	4.857 4.856	.00122 .00120	2.4709
2	1 2	4.885 4.881	.00122 .00122	4.872 4.871	.00120 .00121	2.4816
3	$rac{1}{2}$	4.894 4.894	.00134 .00124	4.884 4.883	.00121 .00120	2.4862

Coor CD1-1, silver paint + silver foil

Resonan	t-cavity met	hod		St.	anding-wave	method
т ^о с	ĸ	tan δ		roc	ĸ	tan δ
26.3	4.8593	.00130		23	4.857	.00130
88	4.8772	.00145		100	4.881	.00146
119	4.888	.00157		200	4.913	.00200
131	4.891	.00164		300	4.943	.00307
166.7	4.905	.0018		400	4.975	.00538
210.5	4.919	.00229		500	5.009	.0111
243	4.928	.00243		600	5.046	.0189
265	4.935	.0025		700	5.092	.034
287	4.941	.0035		800	5.142	.060
308	4.955	.0039		900	5.202	.110
327	4.962	.0045			31202	
346	4.971	.0050	∆K/K	0 -	.0917	
373	4.983	.0072	$\frac{\Delta K/K}{\Delta T}$ at	300°C =	4.859 x 273	$\frac{1}{7} = 6.89E-5;$
			$\frac{\Delta K/K}{\Delta T}$ at	900°C =	.345 4.857 x 877	

Cordierite ceramics (cont.)

"Rayceram" QNP 2102

Raytheon

Resonant-cavity method

4.17	GHz (TE111	mode)	8.7	3 GHz (TE113	mode)
TOC	ĸ	tan δ	$\mathbf{T}^{\mathbf{o}}\mathbf{c}$	к	tan δ
20.5	4.7448	.0018	20.5	4.7439	.00165
64	4.7600	.0019	74.7	4.7633	.0019
104.5	4.7767	.0022	100.5	4.7761	.0020
255.3	4.837	.0034	254	4.8335	.0034
334	4.869	_	295	4.8492	.0041
368	4.880	-	374	4.9018	.0052
			414	4.9145	.0057

Standing-wave method

"Rayceram" QNF 2102 in room- temperature holder			At 8.515 GHz				
	κ		T ^O C	ĸ	tan δ		
Pc. 1	4.734	.00154	23	4.736	.00154		
Pc. 2	4.701	.00157	100	4.769	.0020		
Pc. 3	4.714	.00155	200	4.809	.0033		
Pcs. 1/2/3	4.736	.99157	300	4.852	.0047		
			400	4.897	.0063		
			500	4.944	.0082		
			600	4.992	.0102		
			700	5.040	.0124		
			800	5.096	.0152		

Cordierite + 10% TiO₂

Raytheon

8.515 GHz, standing-wave method

TOC		Face	κ	tan S
24	RTH	1	6.277	.00144
24		2	6.272	.00143
28	HTH	2	6.252	.0015
100			6.252	.0217
200			6.280	. 3026
300			6.292	.0041
400			6.314	.0058
500			6.353	.0077
600			6.391	.0101
700			6.425	.0134
800			6.443	.0153

Fe	*	rí	٠	•	Ω

Transtech

retitie	.							II diibeecii
TT-	1105			2.45 GHz				
т ^о с	ε'/ε _ο	tan	δ	Conductivit (mho-cm)	y μ'/μ	o	tan $\delta_{\mathbf{m}}$	Attenuation (dh/cm)
25	12.8	.0008-	+.0005	1.4E-5	16	60	-10.03	13.6
50		.001		1.7E-5	14		- 8.60	11.4
75		.0012		2.E-5	08		-11.0	9.36
100		.0015		2.6E-5	.02		23.8	6.47
125		.0015		2.6E-5	.16		1.34	2.64
150		.0011		1.8E-5	.48		.035	.160
175		.0015		2.65E-5	,80		.0086	.0623
200		.0025		4.46E-5			.0062	.073
250		.0023		1.21E-4	1.03		.0072	.117
300		.0139		2.53E-4	1.03		.0072	.184
350		.0314		5.81E-4			.0094	.344
400		.0314		1.31E-3			.0124	.707
500		.392		7.5E~3	1.00		.028	3.71
000	14.1	. 392		7.36-3	1.00	,	.020	3.71
				1 GHz				
25	12.8	.0005	<u>+</u> .0003	3.6E-6	2.09	97	2.097	7.7
"Fe	rrimag" 5 (24°C, 14 G K' = 20. <u>+</u> 5	Hz	5	<u>-</u> 4, μ'/μ _o =	1.37 <u>+</u> .3	L, tan	δ _m = .024 <u>-</u>	Permag
Germani	um mullite						Genera	l Electric
				24 GHz				
	т ^о с				т ^о с			
	1 0	κ	tan δ		1 6	K	tan δ	
	25	6.92	.0003		450	7.54	.0071	
	77	7.00	.0002		540	7.67		
	100	7.03	.0003		606	7.76		
	180	7.16	.0011		674	7.85		
	300	7.33	.0031		734	7.93		
	375	7.44	.0048		800	8.04		
Lithium	Niobate			24 GHz			MIT L	incoln Lab.
				24 G112				
		E	Y		E	X		

Magnesium fluoride, IRTRAN 1

tan δ

8.5 GHz 23°C

39.

.0054

Eastman Kodak

0.5 GHZ 25

 $\kappa = 5.276$ tan $\delta = .00017$

27.9 .0122

24	GH 2

TOC	κ	tan δ	TOC	ĸ	tan δ
25.3	5.29	.0001	367	5.78	.0006
53	5.33	.0001	451	5.93	.0007
104	5.39	.0001	517	6.06	.0009
146	5.45	.0002	597	6.23	.0013
194	5.52	.00025	654	6.36	.0022
239	5.57	.00035	722	6.6	.060
293	5.66	•U005			

Sialons and Silicon nitride

AFML (Ruh)

 $Si_3N_4 + 6\% CeO_2 + 15\% BN$ 180090; vacuum bot-pressed

1800°C vacuum hot-pressed, 20 Dec. 1977, density=2.866 g/cm³ 1900°C vacuum hot-pressed, Jan. 1978, density=2.848 g/cm³

14 GHz

Face	Rotation (degrees)	T ^O C	κ	tan δ	Face	Rotation (degrees)	T ^O C	к	tan δ
1	0 90	22 22	7.175 7.157	.00966 .00931	1	0 90	22 22	7.166 7.131	.0131
. 2	0 90	22 22	7.159 7.148	.00935 .00875	2	0 90	22 22	7.144 7.173	.0133 .0134
1	0	100 200 300 400 500 600	7.25 7.35 7.45 7.58 7.72 7.88	.0125 .0180 .0247 .0357 .0475	1	0	100 200 300 400 500 600	7.22 7.32 7.42 7.53 7.65 7.78	.0154 .0210 .0249 .0415 .0548

G.E. 128-2

1100

1150

1200

1220

1250

1270

General Electric

Standing-wave measurements at 24 GHz

Re	sonant-ca	avity	measurements
at	approx.	8.5	GHz

8.51 8.57

8.62

8.65

8.70

8.75

TOC	κ	tan δ	T ^O C.	κ	$\texttt{tan} \ \delta$
25	7.67	,0014	25	7.65	.0028
100	7.72	.0014	100	7.67	.0022
200	7.78	.0015	200	7.69	.0024
300	7.85	.0015	300	7.73	.0025
400	7.91	,0015	400	7.78	.0026
500	7.97	,0015	500	7.84	.0027
600	8.05	.0015	600	7.89	.0027
700	8.13	.0016	700	7.95	.0026
800	8.21	.0017	800	8.02	.0025
900	8.30	.0017	25	7.76	.0019
1000	8.40	.0021			, , , ,

-23-

.0026

.0030

.0037

.0040

.0098

Sialons and Silicon nitride (cont.)

•	**	4 /	• ^	1
	F.,	14	4	-1

General Electric

tan δ
.0016
.0022
.0028
.0031
.0031
.0032
.0033

Resonant-cavity	measurements
at approx. 8.5 (GHz

Standing-wave measurements at 24 GHz

т ^о с	K	tan δ	T ^O C	ĸ
25	7.79	.0015	25	7.67
100	7.815	.0016	100	7.68
200	7.86	.0017	200	7.70
300	7.91	.0017	300	7.73
400	7.97	.0018	400	7.77
500	8.03	.0019	500	7.82
600	8.09	.0020	600	7.87
700	8.16	.0021	700	7.94
800	8.22	.0022	800	8.01
900	8.30	.0023		
1000	8.37	.0026		
1100	8.46	.0030		
1150	8.50	.0033		
1200	8.57	.0038		
1260	8.67	.014		

G.E. 130-1

κ	tan δ	TOC	κ	tan δ
7.44	.0014	25	7.55	.00182
7.48	.0014	100	7.58	.00225
7.53	.0015	200	7.62	.00266
7.58	.0015	300	7.65	.00274
7.62	.0016	400	7.69	.00272
7.66	.0017	500	7.72	.00268
7.71	.0018	500	7.77	.00276
7.75	.0019	700	7.81	.00292
7.81	.0020	800	7.87	.0031
7.87	.0022			
7.93	.0025			
8.02	.0040			
8.08	.0057			
	7.44 7.48 7.53 7.58 7.62 7.66 7.71 7.75 7.81 7.87 7.93 8.02	7.44 .0014 7.48 .0014 7.53 .0015 7.58 .0015 7.62 .0016 7.66 .0017 7.71 .0018 7.75 .0019 7.81 .0020 7.87 .0022 7.93 .0025 8.02 .0040	7.44 .0014 25 7.48 .0014 100 7.53 .0015 200 7.58 .0015 300 7.62 .0016 400 7.66 .0017 500 7.71 .0018 500 7.75 .0019 700 7.81 .0020 800 7.87 .0022 7.93 .0025 8.02 .0040	7.44 .0014 25 7.55 7.48 .0014 100 7.58 7.53 .0015 200 7.62 7.58 .0015 300 7.65 7.62 .0016 400 7.69 7.66 .0017 500 7.72 7.71 .0018 500 7.77 7.75 .0019 700 7.81 7.81 .0020 800 7.87 7.87 .0022 7.93 .0025 8.02 .0040

Silica

1200

Corning 7940 (1979), 8.5 GHz

.0100

8.18

Corning

In room-temperature sample holder

Samples	κ	tan δ
1 pc.	3.825	.00012 + .00003
2 pcs. stacked	3.816	.00010 + .00002
3 pcs. "	3.815	$.00010 \pm .00003$
4 pcs. "	3.820	$.000122^{-} + .000012$

Silica (cont.)

Corning 7940 (cont.)

Corning

Temperature run, 2 pcs. stacked		Temperature run, 3 pcs. stacked			
T ^o C	κ	tan δ	т ^о с	ĸ	tan δ
22	3.815	.0001 + .0001 00005	19.6	3.812*	.00014 <u>+</u> .00005
104	3.819		100	3.816	.00012
165	3.823		207	3.822	.00010
222	3.829		300	3.829	.00011
326	3.837		422	3.829	.00010
410	3.843		488	3.847	.00011
510	3.853		572	3.847	.00011
61.1	3.862		656	3.862	.00011
699	3.879		722	3.879	.00010
751	3.882		750	3.882	.00013

 $[\]star$ Not corrected for stacking error.

Temperature run, 4 pcs. stacked		Previo	ous resonant	-cavity data [†]	
т ^о с	K**	tan δ	TOC	ĸ	tan δ
25.3	3.822	$.00014 \pm .0003$	25	3.823	$.00015 \pm .00007$
100	3.827	.00011	100	3.829	.00014
200	3.835	.00010	200	3.836	.00012
297	3.844	.00010	300	3.845	.00012
400	3.855	.00010	400	3.855	.00012
493	3.866	.00012	500	3.866	.00012
600	3.878	.00013	600	3.878	.00012
725	3.894	.00014	700	3.890	.00012
760	3.900	.00014	800	3.904	.00013
800	3.905	.00014			
25.0	3.823	.00014			

^{**}Corrected for stacking error.

 $^{^{\}dagger}$ Corrected for thermal expansion and frequency shift from 4 to 8.5 GHz.

Slip cast with moisture proofing, 8.5 GHz			Harbisc	n-Walker	
$\mathbf{r}^{\mathbf{o}}\mathbf{c}$	κ	tan δ	T ^O C	κ	tan 6
22	3.224	.00075	600	3.281	.00250
1.00	3.233	.00095	700	3.293	.00335
200	3.242	.00092	800	3.304	.0042
300	3.247	.00090	900	3.317	.0050
400	3.257	.00140	22	3.198	.00054
500	3.268	. 00180			

Si	lica	. (c	ont	٠,
U.L.	T rr-0	, , _	ouc	. ,

Side of	•		ילחו/ מוחו)\ 0 E	Cu-			Drum and ale
_	ast, bru	nswick 2	201B (1978	5), 8.3	GHZ			Brunswick
TOC	ĸ	tan	δ		T	^о С	K	tan ô
22	3.460	.001	.04		6	50	3.481	.00042
100	3.471	.000	080			00	3.480	.00049
200	3.475	.000)50		7	50	3.479	.00058
300	3.475	.000	35		8	00	3.482	.00068
400	3.474	.000	28		9	00	3.490	.00090
500	3.477	.000				71	3.456	.00016
600	3.481	.000)37			57	3.450	.00024
Silica	Composi	te ADL-4	D6 (1.59g	gm/cc)				measured under AG46-79-C-0047;
Af	ter preh	neat to	700 ⁰ C					-45(August, 1979)
8.	5 GHz,		cont	inued				received`
ToC	κ	tan 6	т ^о с	K	tan δ	т°С	K K	tan δ
22	2.656	.00153	503	2.673	.00062	24	2.878	.0072
1 hour			587	2.684	.00092	117	2.878	.0072
22	2.660	.00218	735	2.703	.00120	217	2.856	.0033
67.5	2.658	.00202	790	2.709	.00132	271	2.841	.0023
83.5	2.657	.00185	835	2.714	.0016	320	2.833	.0016
116.6	2.655	.00093	973	2.726	.0028	404	2.823	.0018
123	2.654	.00083	1100	2.736	.0032	496	2.813	.0020
190	2.650	.00079	1178	2.741	.0036	546	2.809	.0021
252	2.649	.00061	1234	2.746	.0040	698	2.797	.0022
300	2.652	.00061	1290	2.77	.0045	750	2.793	.0023
411	2.663	.00120	1321	2.79	.0048	800	2.790	.0023
429	2.665	.00086	1400	2,82	.0057	95	2.822	.0020
8.	5 GHz, 1	Mode 2						
22	2.8295	.00196	623	2.832	.00079			
130		.00122	731	2.835	.00126			
189	2.826	.00086	1016	2.860	.00302			
Silicates								
Cornin	g 9754 g	lass						Corning
8	.515 GHz	;					24 GHz	
$\mathtt{T}^{\mathbf{o}}C$	κ	ŧ	an δ		1	C ^O C	κ	tan δ
22	8.72	(0069			23	8.69	.0089
100	8.91		0069				8.83	.0090
200	9.18		0070				9.05	.0093
300	9.47		0072				9.29	.0097
400	9.78		0074				9.55	.0103
500	10.08		0079				9.83	.0108
600	10.4	.(0085				10.14	.0116

S

8-3A

1

0 90

-27-

7.840 7.828

.467 .440

Silicates (co	nt.)					
"Cervit"	Glass-1, 8.5	15 GHz			Owens-	Illinois
т ^о с	κ	tan δ	т ^о с	κ	tan δ	
22 100 200 300	6.38 6.87 7.37 7.85	.050 .066 .081 .097	400 444 538	8.52 8.88 9.12	.145 .184 .346	
Silicon carbi	.de				Vesuvius (Crucible
	ninal measure s conductivi	ements on samp ties	les			
	Sample	R	esistivity	in ohm-cm		
	designation	100 Hz	1 k ł	iz 10	kliz	
	NR2 NH1 LR1 LH1	.661 .06414 .004593 .003604		92 .0	58 6377 04509 03587	
Silicon carbi	.de + glass π	atrix			ITT G1	lf illa n
May stone	.25, 2.45	Hz				
т ^о с	κ	tan δ	T ^O	с к	tan 6	
25	25.6	.247	300	29.5	.0983	
100	26.2	.275	400			
150	27.2	.239	450			
200 250	28.7 29.4	.115 .0956	500	29.4	.127	
		Repea	t run			
25	25.6	.190	250	29.3	.0955	
100	26.2	.154	300			
200	28.7	.101	400			
Silicon nitri	lde			Sample	es from AMMRC	
sintered,	8,515 GHz					
Sample	Face	Rotation (degrees)	T ^O C	κ	tạn đ	
HP-X-214	1	0	25	8.653	.00744	
	n	90		8.646	.00735	
	2	0 90		8.586 8.590	.00655 .00654	
7-24	1	0		7.787	.0229	
	_	90		7.742	.0214	
	2	0		7.455	.0226	
0.24	•	90		7.511	.0262	

Silicon nitride (cont.)

Hot-pressed,	sample	HP-X-214,	8.515	GHz
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AMMRC

T ^O C	κ	tan δ	$\mathbf{T}^{\mathbf{O}}\mathbf{C}$	κ	tan δ
23.5	8.63	.0064	493	9.17	.0067
100	8.70	.0066	596	9.30	.0065
207	8.81	.0065	679	9.40	.0064
290	8.92	.0065	700	9.44	.0066
395	9.06	.0070	752	9.50	.0067

Ceralloy 147Y-1, 24 GHz

Ceradyne

Measurements in room-temperature sample holder

Sample	Face	Rotation (degrees)	к	tan δ
A	1.	0	8.79	.00363
	2	0	8.73	.00894
	2	45	8.83	.00354
	2	135	8.72	.00746
В	1	0	8.26	.00166
	1	45	8.27	.00452
	1	135	8.42	.00385
	2	0	8.25	.0015
	2	90	8.39	.0093

Temperature runs

	A, Face 1,	0°	E	, Face 1,	00
T°C	κ	tan δ	T^OC	κ	tan ô
25	8.79	.0036	25	8.26	.0016
100	8.84	.0041	100	8.30	.0017
200	8.90	.0047	200	8.38	.0019
300	8.97	.0056	300	8.47	.0023
400	9.05	.0061	400	8.56	.0024
500	9.14	.0063	500	8.66	.0023
600	9.23	.0061	600	8.77	.0031
700	9.33	.0062	700	8,88	.0048
750	9.38	.0075	750	8.93	.0057
800	9.44	.0091	800	8.99	.0067

Silicon nitride

Chemical vapor deposition, specimen No. 231 General Electric/RSD Measured at 24GHz under AMMRC Contract No. DAAG46-79-C-0096; reference AMMRC TR-81-45(March 1982) 24 GHz

т ^о с	κ	tan δ	T ^o C	κ	tan ô
28.5	8.07	.0003	495	8.64	.0004
99	8.13	<.0003	460	8.73	.0004
208	8.24		624	8.82	.0004
294	8.34		650	8.87	.0004
358	8.44		696	8.95	.0005
414	8.53	<.0004	733	6.01	.0005

Silicon nitride plus BN fibers

AVCO

Sample 1 at room temperature

Against short κ' = 9.40; tan δ = .118 $\lambda/4$ away κ' = 9.00; tan δ = .144

Temperature run, average

$\mathbf{T}^{\mathbf{O}}\mathbf{C}$	κ	tan δ	т ^о с	κ	tan δ
25	9.15	.131	500	9.33	.137
100	9.18	.132	600	9.38	.137
200	9.21	.135	700	9.53	.138
300	9.25	.136	800	9.47	.139
400	9.30	.137	•		

Sample 2 at room temperature

Against short $\kappa' = 9.25$; tan $\delta = .125$

 $\lambda/4 \text{ away} \qquad \kappa^1 = 8.69; \ \tan \delta = .144$

Calculated as a magnetic sample:

 $\kappa' = 8.04$; tan $\delta_d = .9215$; $\mu'/\mu_0 = 1.12$; tan $\delta_m = .121$

Silicon mullite, ceramic

General Electric

8.5 GH	z, density	= 3.15 g/cm ³	24 GHz,	24 GHz, 3.12 g/cm ³		
т ^о с	κ	tan δ	т ^о с	κ	tan δ	
23	7.02	.0004	23,5	6,98	,0002 + .0001	
83	7.09	.0005	. 111	7,04	.0003	
207	7.21	.0008	2.3	7.14	.0004	
357	7.40	.0023	276	7.22	.0012	
440	7.55	.0043	374	7.34	.0032	
534	7.60	.0062	460	7.46	.0070	
573	7.75	.0067	554	7.59	.0138	
632	7.84	.0072	607	7.66	.0177	
69 8	7.95	.0073	660	7.73	.023	
740	8.01	.0073	719	7.82	.030	
800	8.12	.0072	740	7.86	.033	

0	_	GHz
8		UNZ

	T ^O C	Density (g/cm ³)	к	tan δ	
Pressed pellet	23	1.683	3.28	.00005 <u>+</u> .00001	
Fast cooled from liquid	23	1.976	3.78	.00005 <u>+</u> .00001	
Pressed pellet (m.p. 120°C)	23		3.379	.000046	
Liquid (b.p. 447°C)	48 65 88 101 126.7 125 140 160 180 200		3.378 3.378 3.379 3.375 3.289 3.38 3.38 3.38 3.39 3.40	.000062 .000052 .000008 .00012 .00038 .0004 .0007 .0005 .0006	÷ 4
	220 240 260		3.40 3.41 3.41 3.38 3.33 3.28 3.24 3.20 3.17 3.14	.0007 <.002 <.004	

Zinc sulfide

Eastman Kodak

(IRTRAN 2), 8.5 GHz, 24° C, density = 4.081 g/cm^3

 $\kappa' = 8.43$; tan $\delta = .00160$

24 GHz

тос	K	tan δ	т ^о с	ĸ	tan S
25	8.32	.00170	600	9.32	.0069
100	8.44	.00172	650	9.56	.0148
200	8.61	.00175	700	9.75	.0244
300	8.79	.0019	730	9.92	.033
400	9.00	.0025	750	10.03	.037
500	9.24	0029			

Zirconia fiber products

Zircoa

24 GHz, 24°C

•	κ	tan 6
"ZIRCAR" Type "ZIRCAR" Type	2.63 1.474	.0082
	 -30	

"Pyroceram"9606

Corning

Measurements on a group of 12 samples received in December 1977 from General Dynamics and one sample from Raytheon

Standing-wave measurements at $8.515~\mathrm{GHz}$, $24^{\circ}\mathrm{C}$

		Face 1			Face 2		
Sample No.	Diameter (inches)	к	tan δ	Diameter (inches)	к	tan ô	Density (g/cm ³)
1 BH	.9993	5.5426	,00023	.9996	5.5418	.00022	
1 OP		5.5457	.00020		5.5436	.00022	
2 BH	1.0005	5.5382	.00018	1.0007	5.5389	.00018	
3	1.0004	5.5430	.00020	1.0003	5.5431	.00019	
4	.9992	5.5395	.00021	.9994	5.5405	.00021	
5	.9998	5.5456	.00020	.9998	5.5465	.00020	
6.	.9993	5.5481	.00022	.9993	5.5457	.00020	2.5933
7	.9996	5.5396	.00021	.9997	5.5414	.00022	
8	1.0000	5.5421	.00021	1.0003	5.5415	.00021	2.5914
9	.9998	5.5446	.00021	1.0000	5.5442	.00021	2.5929
10	1.0003	5.5428	.00021	1.0005	5.5448	.00021	2.5927
11	.9987	5.5359	.00023	.9992	5.5362	.00022	2.5898
12	.9997	5.5469	.00021	.9997	5,5461	.00020	2.5922

RH - Sample measured against bottom of sample holder.

OP - Sample measured a quarter wavelength from end using a polystyrene tube spacer.

Resonant-cavity measurements at approx. 8.5 GHz

#1		#2	2	#3		#4				
T ^o f	ĸ	tan 6	$T^{O}F$	κ	tan δ	ĸ	tan δ	$T^{O}F$	κ	tan δ
67	5.542	.00023	69	5.539	.00020	5.543	.00020	74	5.540	.00021
300	5.586	.0003	300	5.581	.00029	5.585	.00030	300	5.584	.0004
600	5.643	.0007	600	5,635	.0008	5.639	.0008	600	5.636	.0010
900	5.714	.0021	. 900	5.701	.0014	5.712	.001 6	900	5.713	.0018
1200	5.80	.0052	1200	5.784	.0045	5.79	.0045	1200	5.785	.0054
	i	∦ 5		#	7	#	8		#9	
72	5.546	.0002	72	5.541	.0002	5.342	.0002	72	5.544	.0002
300	5.588	.0004	300	5.586	.0003	5.584	.0004	300	5.589	.0004
600	5.646	.0010	600	5.647	.0006	5.643	.00115	600	5.649	.0012
900	5.710	.0015	900	5.709	.0014	5.710	.0023	900	5.713	.0028
1200	5.793	.0045	1200	5.781	.0052 -31-	5.790	.0043	1200	5.786	.0056

"Pyroceram"9606 (cont.)

Resonant-cavity measurements at approx. 8.5 GHz (cont.)

		#10			#12			
		TOF	κ	tan S	TOF	κ	tan ô	
		72	5.544	.0002	70	5.546	.0002	
		300	5,589	.0004	300	5.589	.0004	
		600	5.649	.0008	600	5.646	.0010	
		900	5.715	.0018	900	5.714	.0021	
		1200	5.792	.0059	1200	5.798	.0058	
		#11		#6			Raytheon	
T ^o F	κ	ta	nδ	ĸ	tan δ		κ	tan 6
74	5.536	.000	22 <u>+</u> 5	5.547	.00022	<u>+</u> 5	5,661	.0003 ± 1
300	5.581	.000	28 <u>+</u> 5	5.587	.00030	<u>+</u> 5	5.697	.0005 <u>+</u> 1
600	5.643	.000	7 <u>+</u> 2	5.642	.00053	<u>+</u> 7	5.751	.0010 <u>+</u> 2
900	5.718	.001	8 <u>+</u> 4	5.708	.0014 <u>+</u>	2	5.808*	.0019* ± 4

5.79

.0042 <u>+</u> 4

Error in right digit shown for tan δ Error in \times \pm .002 except at $1200^{O}F$ \pm .03

 $.0041 \pm 5$

5.81

1200

Average values for 12 samples from Gen. Dynamics

Dec.	1977,	densities:	2.5898 to	2.5933	gm/cm	From 1	Raytheon	Nov. 19	/9
		8.5 GHz					8.5 GHz		
T°F	T°C	К	D.F.		T°F	T°C	ĸ	D.F.	
					73	22.6	5.619	.00028	
73	23	5.542	.00021		212	100	5.649	.00033	
					392	200	5.683	.00060	
300	149	5.586	.0003		572	300	5.720	.00105	
					752	400	5.760	.00165	
600	316	5.643	.0009		932	500	5.804	.00263	
					1112	600	5.847	.00388	
900	482	5.711	.0018		1292	700	5.888	.00567	
					1400	760	5.915	.0070	
1200	649	5.79	.0049		1472	800	5.932	.0082	
_									

^{*}Extrapolated from run to 752°F

"Pyroceram" 9606, continued

From	Gen.	Dynamics	July	1978:
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	8.5 GHz					
T°C 22.3 100 200 299	K 5.419 5.453 5.501 5.549	D.F. .00030 .00047 .00069	"Pyroce	eram" 960Q		Corning
400 5.601 500 5.661	.00139 .00197		from Gen.	Dynamics	July 1978	
600	5.725	.00294		8.5	GHz	
700 750	5.781 5.814	.00469	T°F	T°C	ĸ	D.F.
810	5.864	.00734	73	23	6.268	.00024
			122	50	6.259	.00022
			176	80	6.254	.00022
			212	100	6.257	.00024
			248	120	6.262	.00026
			284	140	6.270	.00029
			338	170	6.282	.00033
			392	200	6.296	.00042
			572	300	6.334	.00050
			752	400	6.377	.00098
			932	500	6.424	.00236
			1112	600	6.477	.0044
			1292	700	6.542	.0074
			1472	800	6.615	.0113
			1517	825	6.638	.0124

Pyroceram 960Q	Sample	from General	Dynamics	1980	
	8.515 GHz			24 GHz	
T ^O C	κ	tan δ	т°с	ĸ	tan δ
25	6.228	.00027	21	6.173	.00032
100	6.209	.00025		6.157	.0004
200	6.206	.00041		6.164	.0005
300	6.215	.00070		6.179	.0006
400	6.236	.00140		6.198	.0010
500	6.265	.00295		6.227	.0020
600	6.296	.0060		6.275	.0050
700	6.321	.0112		6.338	.013
900	6 25	018		6 40	020

"Puroceren	"Pyroceram" 960Z Corning								
•			1 1070	1			_		
Sample ir	om Gen. Dy	namics Ju.	Ly 19/8	Sampi	Les Irom	Cen. Dynami	CB 1980		
	8.5 GH	Z			8.5 GHz	24 G	Hz		
T°C	К	D.]	₹	T°C	к р	.F. K	D.F.		
23.1 90 150 231 297 350 435 525 585 653 690 730 765 800	5.732 5.771 5.811 5.861 5.901 5.938 5.999 6.064 6.107 6.164 6.188 6.218 6.242 6.272	.000 .000 .000 .000 .001 .001 .002 .003 .005 .006 .008	38 53 74 95 18 69 78 70 50 55	21 100 200 300 400 500 600 700 800	5.853 .0 5.919 .0 5.987 .0 6.054 .0 6.132 .0	0052 5.695 0097 5.743 0208 5.790 0305 5.843 054 5.900 105 5.960	.0008 .0012 .0017 .0028		
Pipe Insul	lating Comp	ound, fre	sh mix	Le	ebanon St	eel Foundry			
		2	.19 GHz						
T°F	K	D.F.	T°F	к	D.F.	C0omposit:	lon:		
77 100 150 200 water 10 300 350 400	14.3 14.3 14.0 13.6 ost, unstab 2.8 1.21 1.21	.15 .18 .22 .24 le .026 .0074 .0079	500 600 700 800 900 1000 1100	1.22 1.23 1.24 1.26 1.28 1.30 1.33	.0096 .012 .016 .021 .028 .040 .056	Perlite SSF Water Silicate ZnO	82 grams 5 grams 23 ml 87 grams 13 grams		

Chimney Flue Liner

Sample from MIT, Melcher

D.C. conductivity (one-minute) versus temperature

T°C	Sigma, mho/cm	T °C	Sigma, mho/cm	т°С	Sigma, mho/cm
22.5	4.40E-13	217.5	2.45E-10	583	5.53E-6
33	3.94E-14	232.6	4.88E-10	653	1.19E-5
55	1.33E-13	281	2.64E-9	704	1.88E-5
85	5.44E-13	302.5	5.11E-9	751	2.95E~5
103.5	1.22E-12	411	1.21E-7	793	4.37E-5
137	5.19E-12	495	5.44E-7	841	6.83E-5
161	1.53E-11	12hrs at	245°C	907	1.24E-4
192	7.42E-11	439	2.08E-7	969	1.90E-4
199	1.13E-10	576	5.04E-6	982	2.05E-4

CHIMNEY FLUE LINER

ι0 00 /Τ	T,DEG.C	FREQ.,HZ	K1	К2	TAN DELTA	SIGMA,MHO/CM
C.3824	22.5	100.	5.254	0.793128	0.150943	0.44063E-10
3.3824	22.5	1000.	5.013	0.190604	0.038022	0.10589E-09
3.3824	22.5	10000.	4.902	0.076039	0.015511	0.42244E-09
3.3824	22.5	100000.	4.728	0.048433	0.010244	0.26907E-08
3.3824	22.5	1000000.	4.677	0.038693	0.008273	0.21496E-07
3.3824	22.5	9500000.	4.586	0.037590	0.008196	0.19839E-06
2.6799	100.0	100.	5.831	0.634580	0.108831	0.35254E-10
2.6799	100.0	1000.	5.316	0.336510	0.063298	0.18695E-09
2.6799	100.0	10000.	5.041	0.157745	0.031295	0.87636E-09
2.6799	100.0	100000.	4.892	0.093367	0.019087	0.51870E-08
2.6799	100.0	1000000.	4.767	0.067494	0.014160	0.37497E-07
2.6799	100.0	9500000.	4.703	0.054057	0.011495	0.28530E-06
2.1135	200.0	100.	11.029	8.651924	0.784484	0.48066E-09
2.1135	200.0	1000.	7.353	2.188744	0.297670	0.12160E-08
2.1135	200.0	10000.	5.963	0.751230	0.125976	0.41735E-08
2.1135	200.0	100000.	5.377	0.330298	0.061433	0.18350E-07
2,1135	200.0	1000000.	5.041	0.176863	0.035083	0.98257E-07
2.1135	200.0	950 0000.	4.872	0.105327	0.021619	0.55589E-06
1.7447	300.0	100.	45.871	216.696243	4.724037	0.12J39E-07
1.7447	300.0	1000.	18.303	30.440948	1.663164	0.16912E-07
1.7447	300.0	10000.	9.921	5.454198	0.549772	0.30301E-07
1.7447	300.0	100000.	6.811	1.675701	0.246042	0.93094E-07
1.7447	300.0	1000000.	5.654	0.607396	0.107423	0.33744E-06
1.7447	300.0	9500000.	5.025	0.275409	0.054803	0.14535E-05
1.4956	400.0	105.	203.086	3021.52686	14.878033	0.16786E-06
1.4856	400.0	1000.	55.502	314.027588	5.657909	0.17446E-06
1.4856	400.0	10000.	20.490	39.550461	1.930255	0.21972E-06
1.4856	400.0	100000.	10.048	7.160682	0.712662	.0.33782E-06
1.4856	400.0	1000000.	6.826	1.731097	0.253602	0.96172E-06
1.4856	400.0	9500000.	5.554	0.569652	0.102563	(.30065E-05
1.2934	500.0	1090.	146.175	1804.77759	12.346718	0.10027E-05
1.2934	500.0	10000.	45.371	232.481750	5.124766	0.12916E-05
1.2934	500.0	100000.	18.036	33.052612	1.832572	0.18363E-95
1.2934	500.0	1000000.	9.184	6.321146	0.688289	0.35117E-05
1.2934	500.0	9500000 .	6.103	1.639059	0.268581	0.86506E-05

8.5GHz 24°C as received, K=4.95, D.F.=.026; dry, K=4.81, D.F.=.012

New Jerse	ey Sand #2, in	itial H ₂ O 4	.25%	Ŋ	M.I.T.,Melche	r
	Sigma, d.c.	conductivi	ty mho/cm			
T° C	Sigma	T°C	Sigma	T°C	Sigma	
28	2.11E-10	48 nou	re drying	475	2.02E-9	
50	3.93E-10	63	2 09E-13	490	4.18E-9	
79	1.01E-11	143	1.02E-13	549	2.20E-8	
95	4.73E-1?	229	7.99E-13	609	1.14E-7	
127	5.97E-13	269	2.61E-12	705	8.65E-7	
146	7.21E-13	328	1.84E-11	747	2.73E-6	
216	1.11E-12	395	1.25E-10	831	4.56E-6	
270	5.28E-12					

"Laminsc" 4123					Ameri.can	Cyanamid
25°C	Freq., MHz	ĸ'	tan o			
	10	3.71	.0167			
	30	3.64				
IL-T001 Absorb	er	C1 a	E A	Vatanda 1		lustries
			from Army Research Ce			ianics
Frequency, GHz	· 1			3	5	8.5
-				39.	36.	35.
tan 6	.104	.091	.102	.1445	.125	.085
u'/u _	4.03	2.84	2.11	1.785	1.064	.85
κ' tan δ μ'/μ tan δ _m	.687	.937	1.20	1.218	1.585	1.29
α, att. db/cm	9.56	16.28	24.5	28.2	41.5	51.6
Ferrite-Epoxy	Resin Mixtu	res				AMMRC
	wt% ferrite					
	1.685 2.	45 3	ς.	Ω 5	1.6	24
κ 4.469 tan δ .0947 μ'/μ ₀ 1.294	4.328 4.	178 3 .1 5	3 4.119	3.950	3.92	3.90
$tan \delta$.0947	.0883	0874 .08	25 .0819	.0620	.0512	.046
μ'/μ _o 1.294	1.219 1.	160 1.12	.979	.963	.989	1.00
tan $\delta_{ m m}$.0669	.1703	1858 .19	84 .190	.0528	.0163	.005
MAG-20 5	0 wt% 20 me	sh magnet	ite			
$κ'$ 25.7 tan $δ$.111 $μ'/μ_0$ 1.75	25.4 24.	2 23.6	23.1	13.1	17.2	23.9
$tan \delta$.111	.109 .	116 .1	.14 .101	.0475	.03	.03
μ'/μ_0 1.75	1.57 1.	44 1.3	7 1.12	.937	.897	103
$tan \delta_m$.276	.325 .	378 .4	23 .515	.579	.49	.30
MAG-65 5	∩ wt% 65 me	sh magnet	ite			
κ' 16.84	16.5 16.	46 16.3	16.25	16.16	18.8%	
tan δ .0624	.0633 .	0624 .0	0656 .075	.091	.0593	*
μ'/μ_0 1.765	1.611 1.	495 1.4	53 1.242	.985	2.149*	
$tan \delta_m$ 203	.254 .	309 .3	326 .36	.419	.0979	*
μ'/μ_0 1.765 tan δ_m 203	freq. = 30	zHM O				
"Nylon" 66						urs and Co.
As Received,						2 days, 68°C
Time, sec. Fr	eq., Hz o m		Time,		eq., Hz	o mho/cm
		6E-11			1000	2.61E-11
	100 3.8	4E-12			100	2.14E-12
	00265 6.9	5E15		:	20	3.17E-13
		5E-15	6	0 .0	00265	7.31E-17
778 .0	00020 2.5	9E~15	12	0 .	00133	5.41E-17
2400 .00	00066 1.6	6E-15	1.8	0 .	00088	3.90E-17
			30		00053	2.98E-17
Frequencies le				$(2\pi t)$; th	is assume	s charging
current is neg	ligible at	these tim	. 89u			

E. I. Dupont de Nemours and Co. Sample molded by AMP

Water Content = .13%

T, DEG.C	FREQ.,HZ	H 1	K2	TAN DELTA	SIGMA.MHD/CM
00000000000000000000000000000000000000	10. 20. 30. 50. 100. 200. 300. 500. 1000. 2000. 3000. 5000. 10000. 20000. 30000. 50000. 100000. 30000. 50000.	3.647 3.647 3.6638 3.5566 3.5566 3.5564 3.5443 3.4408 3.370 3.3305 3.3297 3.2247 3.2248 3.2248 3.2248 3.2248	0.017556 0.019707 0.021817 0.023715 0.027065 0.038884 0.042309 0.048911 0.064390 0.064390 0.067870 0.073324 0.073324 0.073176 0.073176 0.073176 0.069027 0.067859 0.067459 0.067459 0.067459 0.067161 0.066853 0.066853	0.004794 0.005404 0.005990 0.006528 0.007480 0.010875 0.011863 0.013727 0.015141 0.018323 0.019484 0.021296 0.022619 0.023238 0.022521 0.021923 0.020888 0.020585 0.020620 0.019468 0.020345 0.020345 0.020990 0.021019 0.021019	0.97532E-13 0.21896E-12 0.36362E-12 0.65876E-12 0.15036E-11 0.43204E-11 0.70515E-11 0.13586E-10 0.29826E-10 0.71545E-10 0.11312E-09 0.42766E-09 0.42766E-09 0.42766E-09 0.1305E-07 0.1369E-07 0.1369E-07 0.1369E-07 0.1369E-07 0.1369E-07 0.1369E-07 0.22284E-06 0.22284E-06 0.35086E-06
		3.145	0.067829	0.021566	0.11305E~05

Water Content = .23%

T, DEG.C	FREQ.,HZ	K 1	K;	TAN DELTA	SIGMA, MHD/CM
25.0 25.0	5.	4.413	0.108300	0.024539	0.30083E-12
25.0	10.	4.364	0.102985	0.023598	0.57214E-12
25.0	20.	4.316	0.098521	0.022.36	0.10947E-15
25.0	30.	4.285	0.098263	0.022932	0.16377E-11
	50.	4.229	0.098553	0.023304	0.27376E-11
25.0	100.	4.208	0.101789	0.024190	0.56549E-11
25.0	200.	4.119	0.123972	0.030094	0.13775E-10
25.0	300.	4.117	0.127763	0.031036	0.212946-10
25.9	500.	4.067	0.135662	0.033354	0.37684E~10
25.0	1000.	4.014	0.143965	0.035868	0.79981E-10
25.0	2000.	3.957	0.148788	0.037600	0.16532E-09
25.0	3000.	3.918	0.154694	0.039479	0.25782E-09
25.0	5000.	3.868	0.155900	0.040306	0.43306E-09
25.0	10000.	3.795	0.160411	0.042272	0.89117E~09
25.0	20000.	3.724	0.158407	C.042539	U.17601E-08
25.0	50000.	3.635	0.151328	0.041632	0.42035E~08
25.0	100000.	3.574	0.141872	0.039696	0.78818E~08
25.0	200000.	3.507	0.128033	0.038510	0.14226E~07
25.0	300000.	3.477	0.121737	0.035018	
25.0	500000.	3.450	0.113173	0.032808	0.20290E~97
25.0	1000000.	3.378	0.103135	0.030535	0.31437E~07
25.0	2000000,	3.358	0.091325	0.027198	0.57297E-07
25.0	3500000.	3.324	0.085876	0.025836	0.10147E-06
25.0	60000000.	3.297	0.083500		0.16698E~06
25.0	9500000.	3.275	0.078812	0.025323	0.27833E-06
25.0	30000000.	3.259	0.072724	0.024063 0.022316	0.41595E-06 0.12121E-05

T°C K D.F T°C K D.F.	AL-300, p	olyimide	laminate	1			Atlantic	Laminates
26				8.5	GHz			
48		T°C	K	D.F	T°C	ĸ	v.r.	
48		26	4.65	.0192	179	4.64	.0238	
71		48	4.71	.0203	21.2			
96		71	4.69					
123		96						
"Avcoat" 8029 Thickness (cm) T°C K D.F. (cm) T°C K D.F. 3.189 25 2.267 .00079 3.228 25 3.202 60.5 2.257 .00079 reheated 3.210 108 2.244 .00101 3.469 348 2.019 .0022 3.215 136 2.234 .00116 3.949 406 1.896 .00235 3.241 189 2.214 .00130 4.197 450 1.805 .00218 3.276 224 2.198 .00148 4.415 485 1.756 .00200 3.377 278 2.160 .00172 5.037 509 1.44 .0027 3.432 300 2.142 .00188 liquid with bubbles 3.771 343 2.055 .0021 AVCO K96 sample one		123	4.72					
Thickness (cm) T°C K D.F. (cm) T°C K D.F. 3.189 25 2.267 .00079 3.228 25 3.202 60.5 2.257 .00079 reheated 3.210 108 2.244 .00101 3.469 348 2.019 .0022 3.215 136 2.234 .00116 3.949 406 1.896 .00235 3.241 189 2.214 .00130 4.197 450 1.805 .00218 3.276 224 2.198 .00148 4.415 485 1.756 .00200 3.377 278 2.160 .00172 5.037 509 1.44 .0027 3.432 300 2.142 .00188 liquid with bubbles 3.771 343 2.055 .0021 AVCO K96 sample one 8.5 GHz E perpendicular to hot pressing dir. bot pressing dir. T°C K tan & Thickness K tan & Cm) 20.3 2.464 .00207 1.9350 2.383 .00160 64.3 2.453 .00203 1.9424 2.375 .00187 101 2.441 .007 10 1.9504 2.362 .00173 148 2.452 .00212 1.9559 2.351 .00165 203 2.3406 .00221 1.9711 2.326 .00091 250 2.347 .00229 2.0239 2.255 .00115 303 2.056 .00221 1.9711 2.326 .00091 250 2.347 .00239 2.0239 2.265 .00115 303 2.056 .00250 2.3077 1.980 .00133 347		148						
Thickness (cm) T°C K D.F. (cm) T°C K D.F. 3.189 25 2.267 .00079 3.228 25 3.202 60.5 2.257 .00079 reheated 3.210 108 2.244 .00101 3.469 348 2.019 .0022 3.215 136 2.234 .00116 3.949 406 1.896 .00235 3.241 189 2.214 .00130 4.197 450 1.805 .00218 3.276 224 2.198 .00148 4.415 485 1.756 .00200 3.377 278 2.160 .00172 5.037 509 1.44 .0027 3.432 300 2.142 .00188 1iquid with bubbles 3.771 343 2.055 .0021 AVCO K96 sample one	"Avcoat"	80 29						AVCO
Cem	meta i ata a	•		8.5	GHz			11 " 00
3.189			,,		Thickne	88		
3.202 60.5 2.257 .00079 reheated 3.210 108 2.244 .00101 3.469 348 2.019 .0022 3.215 136 2.234 .00116 3.949 406 1.896 .00235 3.241 189 2.214 .00130 4.197 450 1.805 .00218 3.276 224 2.198 .00148 4.415 485 1.756 .00200 3.377 278 2.160 .00172 5.037 509 1.44 .0027 3.432 300 2.142 .00188 liquid with bubbles 3.771 343 2.055 .0021 AVCO K96 sample one 8.5 GHz E perpendicular to bot pressing dir. T°C K tan δ Thickness K tan δ (cm), 20.3 2.464 .00207 1.9350 2.383 .00160 64.3 2.453 .00203 1.9424 2.375 .00187 101 2.441 .0C^10 1.9504 2.362 .00173 148 2.432 .00212 1.9559 2.351 .00165 203 2.406 .00221 1.9711 2.326 .00091 250 2.347 .00239 2.0239 2.265 .00115 303 2.056 .00250 2.3077 1.980 .00133	-				• •	T°C	K	D.F.
3.210 108 2.244 .00101 3.469 348 2.019 .0022 3.215 136 2.234 .00116 3.949 406 1.896 .00235 3.241 189 2.214 .00130 4.197 450 1.805 .00218 3.276 224 2.198 .00148 4.415 485 1.756 .00200 3.377 278 2.160 .00172 5.037 509 1.44 .0027 3.432 300 2.142 .00188 liquid with bubbles 3.771 343 2.055 .0021 AVCO K96 sample one								
3.215					r	eheated		
3.241 189 2.214 .00130 4.197 450 1.805 .00218 3.276 224 2.198 .00148 4.415 485 1.756 .00200 3.377 278 2.160 .00172 5.037 509 1.44 .0027 3.432 300 2.142 .00188 liquid with bubbles 3.771 343 2.055 .0021 AVCO K96 sample one 8.5 GHz E perpendicular to bothot pressing dir. T°C						348	2.019	.0022
3.276					3.949	406	1.896	.00235
3.377 278 2.160 .00172 5.037 509 1.44 .0027 3.432 300 2.142 .00188 liquid with bubbles 3.771 343 2.055 .0021 AVCO K96 sample one 8.5 GHz E perpendicular to hot pressing dir. T°C						450	1.805	.00218
3.432 300 2.142 .00188 liquid with bubbles 3.771 343 2.055 .0021 AVCO K96 sample one 8.5 GHz E perpendicular to hot pressing dir. TOC K Lan & Thickness K tan & Comp. 20.3 2.464 .00207 1.9350 2.383 .00160 64.3 2.453 .00203 1.9424 2.375 .00187 101 2.441 .00010 1.9504 2.362 .00173 148 2.432 .00212 1.9559 2.351 .00165 203 2.406 .00221 1.9711 2.326 .00091 250 2.347 .00239 2.0239 2.265 .00115 303 2.056 .00250 2.3077 1.980 .00133 **Toc K tan & Thick, cm Toc C & Tan & T						485	1.756	.00200
3.771 343 2.055 .0021 AVCO K96 sample one 8.5 GHz E perpendicular to hot pressing dir. T°C κ tan δ Thickness κ tan δ (cm), 20.3 2.464 .00207 1.9350 2.383 .00160 64.3 2.453 .00203 1.9424 2.375 .00187 101 2.441 .00 \text{``10} 1.9504 2.362 .00173 148 2.432 .00212 1.9559 2.351 .00165 203 2.406 .00221 1.9711 2.326 .00091 250 2.347 .00239 2.0239 2.265 .00115 303 2.056 .00250 2.3077 1.980 .00133 347 **Example two, E perpendicular to hot pressing direction T°C κ tan δ Thick.cm T°C κ tan δ Thick.cm T°C α.2 2.448 .00150 2.2110 288 2.368 .00143 2.3187 57 2.443 .00136 2.2200 325 2.365 .00145 2.3522 84 2.436 .00140 2.2295 350 2.033 .00133 2.8405 101 2.431 .00132 2.2356 380 1.951 .00204 2.9830 130 2.424 .00130 2.2452 400 1.431 .00201 3.3168 148 2.418 .00127 2.2533 431 1.879 .00190 3.3124 188 2.399 .00100 2.2682 474 1.843 .00208 3.4829 208 2.390 .00112 2.2797 509 1.645 .00273 3.7028								.0027
AVCO K96 sample one 8.5 GHz E perpendicular to hot pressing dir. TOC K tan & Thickness (cm), 20.3 2.464 .00207 1.9350 2.383 .00160 64.3 2.453 .00203 1.9424 2.375 .00187 101 2.441 .00~10 1.9504 2.362 .00173 148 2.432 .00212 1.9559 2.351 .00165 203 2.406 .00221 1.9711 2.326 .00091 250 2.347 .00229 2.0239 2.265 .00115 303 2.056 .00250 2.3077 1.980 .00133 347 ~ 2.56 sample two, E perpendicular to hot pressing direction ToC K tan & Thick,cm ToC K tan & Thick.cm 20.2 2.448 .00150 2.2110 288 2.368 .00143 2.3187 57 2.443 .00136 2.2200 325 2.345 .00145 2.3522 84 2.436 .00140 2.2295 350 2.033 .00133 2.8405 101 2.431 .00132 2.2356 380 1.951 .00204 2.9830 130 2.424 .00130 2.2452 400 1.431 .00204 2.9830 130 2.424 .00130 2.2452 400 1.431 .00201 3.3168 148 2.418 .00127 2.2533 431 1.879 .00190 3.3124 188 2.399 .00100 2.2682 474 1.843 .00208 3.4829 208 2.390 .00112 2.2797 509 1.645 .00273 3.7028					liqu	uid with	bubbles	
8.5 GHz E perpendicular to hot pressing dir. T ^O C	3.771	343	2.055	.0021				
E perpendicular to hot pressing dir. T ^O C	AVCO K96	sample o	ne	0.5	O**-			AVCO
hot pressing dir. T°C		T			GHZ			
T°C								
Cem	•	HOL	bresarua	dir.		not p	ressing d	ir.
20.3	т ^о С	κ	La	n δ I	hickness	κ	tan 6	5
64.3 2.453 .00203 1.9424 2.375 .00187 101 2.441 .0C 10 1.9504 2.362 .00173 148 2.432 .00212 1.9559 2.351 .00165 203 2.406 .00221 1.9711 2.326 .00091 250 2.347 .00239 2.0239 2.265 .00115 303 2.056 .00250 2.3077 1.980 .00133 347 ~ 2.56 sample two, E perpendicular to hot pressing direction T°C κ tan δ Thick,cm T°C κ tan δ Thick.cm 20.2 2.448 .00150 2.2110 288 2.368 .00143 2.3187 57 2.443 .00136 2.2200 325 2.345 .00145 2.3522 84 2.436 .00140 2.2295 350 2.033 .00133 2.8405 101 2.431 .00132 2.2356 380 1.951 .00204 2.9830 130 2.424 .00130 2.2452 400 1.431 .00201 3.3168 148 2.418 .00127 2.2533 431 1.879 .00190 3.3124 188 2.399 .00100 2.2682 474 1.843 .00208 3.4829 208 2.390 .00112 2.2797 509 1.645 .00273 3.7028				•	(cm),			
64.3 2.453 .00203 1.9424 2.375 .00187 101 2.441 .0C^10 1.9504 2.362 .00173 148 2.432 .00212 1.9559 2.351 .00165 203 2.406 .00221 1.9711 2.326 .00091 250 2.347 .00239 2.0239 2.265 .00115 303 2.056 .00250 2.3077 1.980 .00133 347 ~ 2.56 sample two, E perpendicular to hot pressing direction T°C κ tan δ Thick,cm T°C κ tan δ Thick.cm 20.2 2.448 .00150 2.2110 288 2.368 .00143 2.3187 57 2.443 .00136 2.2200 325 2.345 .00145 2.3522 84 2.436 .00140 2.2295 350 2.033 .00133 2.8405 101 2.431 .00132 2.2356 380 1.951 .00204 2.9830 130 2.424 .00130 2.2452 400 1.431 .00201 3.3168 148 2.418 .00127 2.2533 431 1.879 .00190 3.3124 188 2.399 .00100 2.2682 474 1.843 .00208 3.4829 208 2.390 .00112 2.2797 509 1.645 .00273 3.7028	20.3	2.46	4 .0	0207	1.9350	2.383	.0016	iΩ
101	64.3	2.45	3 .0	0203	1.9424			
148	101			C 10				
203		2.43	2 .0	0212				-
250		2.40	6 .0	0221	1.9711			
303		2.34	7 .0	0239	2.0239			
347		2.05	6 .0	0250	2.3077			
T°C κ tan δ Thick,cm T°C κ tan δ Thick.cm 20.2 2.448 .00150 2.2110 288 2.368 .00143 2.3187 57 2.443 .00136 2.2200 325 2.345 .00145 2.3522 84 2.436 .00140 2.2295 350 2.033 .00133 2.8405 101 2.431 .00132 2.2356 380 1.951 .00204 2.9830 130 2.424 .00130 2.2452 400 1.431 .00201 3.3168 148 2.418 .00127 2.2533 431 1.879 .00190 3.3124 188 2.399 .00100 2.2682 474 1.843 .00208 3.4829 208 2.390 .00112 2.2797 509 1.645 .00273 3.7028	347			~	2.56			-
T°C κ tan δ Thick,cm T°C κ tan δ Thick.cm 20.2 2.448 .00150 2.2110 288 2.368 .00143 2.3187 57 2.443 .00136 2.2200 325 2.345 .00145 2.3522 84 2.436 .00140 2.2295 350 2.033 .00133 2.8405 101 2.431 .00132 2.2356 380 1.951 .00204 2.9830 130 2.424 .00130 2.2452 400 1.431 .00201 3.3168 148 2.418 .00127 2.2533 431 1.879 .00190 3.3124 188 2.399 .00100 2.2682 474 1.843 .00208 3.4829 208 2.390 .00112 2.2797 509 1.645 .00273 3.7028		00mu10	tree E		aulan ta ba	* ***	dma ddwaa	tion
20.2 2.448 .00150 2.2110 288 2.368 .00143 2.3187 57 2.443 .00136 2.2200 325 2.345 .00145 2.3522 84 2.436 .00140 2.2295 350 2.033 .00133 2.8405 101 2.431 .00132 2.2356 380 1.951 .00204 2.9830 130 2.424 .00130 2.2452 400 1.431 .00201 3.3168 148 2.418 .00127 2.2533 431 1.879 .00190 3.3124 188 2.399 .00100 2.2682 474 1.843 .00208 3.4829 208 2.390 .00112 2.2797 509 1.645 .00273 3.7028	mo a							
57 2.443 .00136 2.2200 325 2.345 .00145 2.3522 84 2.436 .00140 2.2295 350 2.033 .00133 2.8405 101 2.431 .00132 2.2356 380 1.951 .00204 2.9830 130 2.424 .00130 2.2452 400 1.431 .00201 3.3168 148 2.418 .00127 2.2533 431 1.879 .00190 3.3124 188 2.399 .00100 2.2682 474 1.843 .00208 3.4829 208 2.390 .00112 2.2797 509 1.645 .00273 3.7028								
84 2.436 .00140 2.2295 350 2.033 .00133 2.8405 101 2.431 .00132 2.2356 380 1.951 .00204 2.9830 130 2.424 .00130 2.2452 400 1.431 .00201 3.3168 148 2.418 .00127 2.2533 431 1.879 .00190 3.3124 188 2.399 .00100 2.2682 474 1.843 .00208 3.4829 208 2.390 .00112 2.2797 509 1.645 .00273 3.7028								
101 2.431 .00132 2.2356 380 1.951 .00204 2.9830 130 2.424 .00130 2.2452 400 1.431 .00201 3.3168 148 2.418 .00127 2.2533 431 1.879 .00190 3.3124 188 2.399 .00100 2.2682 474 1.843 .00208 3.4829 208 2.390 .00112 2.2797 509 1.645 .00273 3.7028								
130 2.424 .00130 2.2452 400 1.431 .00201 3.3168 148 2.418 .00127 2.2533 431 1.879 .00190 3.3124 188 2.399 .00100 2.2682 474 1.843 .00208 3.4829 208 2.390 .00112 2.2797 509 1.645 .00273 3.7028								
148 2.418 .00127 2.2533 431 1.879 .00190 3.3124 188 2.399 .00100 2.2682 474 1.843 .00208 3.4829 208 2.390 .00112 2.2797 509 1.645 .00273 3.7028								
188 2.399 .00100 2.2682 474 1.843 .00208 3.4829 208 2.390 .00112 2.2797 509 1.645 .00273 3.7028								
208 2.390 .00112 2.2797 509 1.645 .00273 3.7028								
					342			

Dielecti	ric i	nsulation	on <u>bo</u> e	rds	230	;		Cincinnat	i Milacro	on
Sample designation	Freq.	Har 1 H	10 H	100 M	300 H	1 G	3 G	8.5 G	14 G	24 G
PC-75	k tan ô	4.14 .0272	3.94 .0358	3.68 .0378	3.64 .0370	3.61 .0324	3.59 .02 8 9	3.568 ± .02 .0245	3.556 .0250	3.54 .026
65H62	κ tan δ	4.40	4.22	3.96 .0415	3.89 .0394	3.81	3.755 .0304	3.715 ± .01 .0256	3.700 .0269	3.685 .029
1/2424	K tan ô	4.49	4.22	3.95	3.89	3.82	3.76	3.710 ± .2 .0300	3.698 .0312	3.68
PR-4*	K tan ô	4.58	4.46	4.33	4.53	4.48	4.46	4.445 ± .02 .0146	4.42 .0150	4.38 .016
HILCLAD CA7FR	K tan ô	4.11	4.02	3.94	3.93	3.92	3,92 ,0105	3.914 ± .01 .0099	3.912 .00985	3.90 .011
CINCLAD NA#	K tan ô	3.86	3.78 .0114	3.69	3.76	3.71	3.675	3.645 ± .01	3.635 .0095	3.625 .0105
CINCLAD MA7FR	K tan 6	4.17	4.09	3.99	3.98 .0126	3.96 .0116	3.94 .0110	3.929 ± .02 .0106	3.917 .0105	3.91 .0108
CINCLAD	K tam ô	4.10	4.01 .0135	3.92	3.89	3.85	3.85	3.839 ± .006		3.82 .0109
	re not	L sheet; high dectropic with 0381 gm/	^{thin 1} i		D.1	7			Industr from Spe	
		3		042	.000،>			-	_	-
		8.5		042)1 <u>+</u> .0	0001			
"Rulon"	II					 .		Dixon	Industr	1es
Freq., Na	DC,	60	100	1 K	24°C, Fre-	4. rus 100 K	1 % 1	ON 16	2.45 G	3 G
	l minut	•								
K ^M tan 6 U mho/em (1 . 31-16 6 . 62-15	3.00 .0103 .00344 3.44H-13	3.00 .0103 .00342 5.78-13	2.99 .00703 .00235 3.908-12	2.99 .00526 .00176 2.928-11	.00462 .00135	.00343	.97 2.863 .00285 .00472 .00096 .00165 .388-8 2.628-6	.00170	2.840 .90517 .00182 8.618-6
					Temperatu	te twa	•			
Freq., GME		1.		10 ⁶ ×		1 43	10 ⁶ x	3.		10 ⁶ ×
T [©] C 26	к' 2.863	K ^M - 00472	.00165		k' k .850 .00	485 ,001	70 6.60	2.840 .00	tan 6	0 8.61
74 109 136 173 203 250 22	2.858 2.854 2.852 2.851 2.855 F.868 2.844	.00903 .00605 .00915 .0151 .0225 .0280 .00435	.00176 .00212 .00321 .00531 .00787 .00975 .00153	3.36 2 5.9 2 8.41 2 12.5 2 15.5 2	.839 .00 .835 .00 .833 .00 .829 .01 .827 .02 .829 .02	641 .002 904 .003 51 .005 16 .007 74 .009	26 8.72 19 12.3 33 20.5 65 29.4 69 37.3		66 -00583, 28 -00811	9.77 12.2 17.5 27.4 38.1 48.4
"Kevlar"	' lam	inates		8.5 GH	z 22°C	E.	I. Dup	ont de Ne Sample	mours an	
	Af	ter 21-1	./2 da	ys 95%	R.H.					
				·ĸ		t.an -δ	;	wt. %		
Fa	ce 1	0		4.	16	.113		4.084		
Fa	ce 1	0		3.	93	.0772	2	3.230		
Fa	ce 1	0		4.	19	.103		4.010		
Fa	ce 1	. 0		3.	78	.0799)	3.485		

#1 #2 #3

11	Kevlar" 1	amin	stes, continue	ed As	Rec	e1ved				
			Against	short				0ν	er λ/4	
Samp	le		Rotation (degrees)	к		tan 8	. ;	111 ₂ 0	ĸ	tan 8
#1	Face Face		0 90 · 0 90	4 - : 4 - : 4 - :	08 05	.0534 .0756 .084 .0819	:	3.505	4.098 4.176	.0707 .0736
#2	Face	e 1	0 90	3. 3.		.0369 .0357	:	2.613		
#3	Fac	e 1	0 90	4. 4.		.0886 .0895		3.677		
#4	Face	e 1	0 90 .		59 72	.0478 .0451		2.784		
		Dr	ied 2-1/2 day	ys 80 ⁰	C va	2. oven				
#1			0 90		35 38	.0092 .0083				
#2			0 90		37 44	.01.09 .0089				
#3			0 90		43 47	.0110				
#4			0 90		20 29	.01.03 .0037				
		45	hours 95%	R.H. De	sicc	ator				
#1			0 90		84 92	.0661 .0672		3.039		
#2			90 ·		62 70	.0318 .0311		2.019		
#3			0 90		79 84	.0500 .0503		2.575		
#4			0 90		60 73	.0465		2.637		
	Intermedi	ate	desiccation		.					
	for Sampl	e #3	;	Hours		ation grees)	κ	tan 6	wt. %	
				69		0 90	3.88 3.93	.0583 .0585	2.931	
				100 139					3.228 3.465	

4

"Kevlar" Ropes

E. I. Dupont de Nemours and Co.

FR is frequency in Hz

Rope A, 24°C, 50% R.H.

FR	K 1	K2	TAN DELTA	SIGMA
50. 100. 1000. 10000. 100000. 9500000.	6.6255 5.9849 5.7568 5.2008 4.7625 4.4191 4.3046 3.6555	0.528094 0.411533 0.334317 0.266940 0.300517 0.303765 0.316421 0.304161	0.079706 0.068762 0.058074 0.051268 0.063100 0.068739 0.073507 0.083207	0.14669E-10 0.22863E-10 0.18573E-09 0.14830E-08 0.16695E-07 0.16876E-06 0.16700E-05

Rope A, 120°C

FR	K1	K2	TAN DELTA	SIGMA
60. 100. 1000. 10000. 100000. 9500000.	21.033 15.918 6.407 4.772 4.560 4.209 4.025	53.21245 29.27719 5.25332 0.85355 0.19611 0.15851	2.52997 1.83929 0.81997 0.17885 0.04301 0.03766 0.04075	0.17737E-08 0.16265E-08 0.29185E-08 0.47419E-08 0.10695E-07 0.88062E-07 0.86569E-08

Rope B, 24°C, 50% R.H.

FR	К1	К2	TAN DELTA	SIGMA
50. 100. 1000. 10000. 100000. 9500000.	7.6933 7.5078 6.9986 6.0960 5.5494 5.1731 4.6283 4.1279	0.875021 0.640551 0.444717 0.323863 0.346957 0.392599 0.406893 0.411350	0.113738 0.085318 0.063543 0.053128 0.062522 0.075892 0.084272 0.099650	0.24306E-10 0.35586E-10 0.24706E-09 0.17992E-08 0.19275E-07 0.21811E-06 0.21475E-05 0.68558E-05

Rope B, 120°C

FR	К1	K2	TAN DELTA	SIGMA
50. 60. 100. 1000. 10000. 100000. 9500000.	26.353 23.345 16.986 5.527 4.982 4.783 4.691 4.588	66.87852 57.07666 39.67288 6.04871 0.78675 0.17227 0.11827	2.53784 2.44490 2.33562 1.09446 0.15793 0.03602 0.02521 0.03222	0.18577E-08 0.19026E-08 0.22040E-08 0.33604E-08 0.43708E-08 0.95707E-08 0.65705E-07

"Kevlar"Ropes, continued

Rope C, 24°C, 50% R.H.

	,			
FR	K1	K2	TAN DELTA	SIGMA
50. 100. 1000. 10000. 100000. 1000000. 9500000.	12.3266 11.6037 9.5361 8.0059 6.8165 5.6022 4.9611 3.9680	1.799829 1.436832 1.285998 0.964711 0.687531 0.653690 0.742388 0.689153	0.146012 0.123825 0.134856 0.120500 0.100863 0.116684 0.149642 0.173678	0.49995E-10 0.79824E-10 0.71444E-09 0.535196E-07 0.36316E-06 0.39182E-05 0.11486E-04
Rope C, 120°	°c			
FR	К1	К2	TAN DELTA	SIGMA
50. 60. 100. 1000. 10000. 100000. 9500000.	36.390 27.560 23.815 7.197 5.520 4.989 4.886 4.441	160.49568 128.04948 89.23180 12.34859 1.78799 0.39323 0.22794 0.27151	4.41044 4.64614 3.74686 1.71576 0.32393 0.07881 0.04665 0.06114	0.44582E-08 0.42693E-08 0.49573E-08 0.68603E-09 0.99333F-08 0.21846E-07 0.12663E-06 0.14329E-05
Rope D, 24°	°С, 50% к.н.			
FR	K1	К2	TAN DELTA	SIGMA
50. 100. 1000. 10000. 100000. 100000. 9500000.	10.3523 10.1137 9.4470 8.0265 6.4284 5.0137 4.5359 3.6717	1.177239 0.912032 0.800575 0.950508 0.921320 0.617431 0.532482 0.476469	0.113718 0.090178 0.084744 0.118422 0.143320 0.123148 0.117392 0.129768	0.32701E-10 0.50668E-10 0.44476E-09 0.52806E-08 0.51184E-07 0.34302E-06 0.28103E-05 0.79412E-05
Rope D, 120	o°c			
FR	К1	K2	TAN DELTA	SIGMA
50. 60. 100. 1000. 10000. 100000. 9500000.	34.260 30.668 22.945 7.334 5.576 5.013 4.956 4.625	127.21927 110.98825 87.83615 10.14525 1.54414 0.33321 0.19092 0.24093	3.71333 3.61901 3.82816 1.38328 0.27692 0.06646 0.03853 0.05209	0.35339E-08 0.36996E-08 0.48798E-08 0.56362E-08 0.85786E-08 0.18512E-07 0.10607E-06 0.12716E-05

```
"Mylar" 2-ply, corragated
                                              E. I. Dupont de Nemours and Co.
             Frequency, MHz
                               K
                                       D.F.
                                      .00507
                             1.114
                  10
                             1.107
                                      .00512
                  20
                             1.106
                                      .00480
                                      .00380
                  30
                             1.106
"Riston", exposed film
                                               E. I. Dupont de Nemours and Co.
    Freq., MHz
                     1
                              10
                                       100
                                                 1000
                                                           8515
                                      2.97
                                                 2.85
                    3.31
                              3.12
                                                           2.77
        D.F.
                                                   .0272
                     .042
                               .039
                                        .0326
                                                            .0182
"Sclair" polyethylene
                                                      Dupont of Canada
         #8307-UV#5
                          24 GHz 22°C
      K = 2.33 \pm .02
                        D.F. = .00027 \pm .00008
      After 1500 hours in Atlas Weatherometer:
      K = 2.30 \pm .02
                        D.F. = .00041 \pm .00003
"Tefze1"
                                               E. I. Dupont de Nemours and Co.
          8.5 GHz 23^{\circ}C K = 2.328 \pm .011
                                              D.F. = .0117
"Eccofloat"
                                                        Emerson and Cuming
                       8.5 GHz 24 °C
    EF38A, .6002 \text{ gm/cm}^3 \text{ K} = 1.8605
                                           D.F. = .0128
    EF38B, .4833 gm/cm<sup>3</sup> K = 1.8401
                                           D.F. ~ .0121
"Eccofoam" HiK 625
                                                           Emerson and Cuming
          24 GHz 24°C
                            K = 6.0
                                        D.F. = .045
"Stycast" 1.9
                                                           Emerson and Cuming
                                                       Sample from MIT, RLE
          8.5 GHz 24°C
                            K = 1.71
                                       D.F. = .0055
"Esscolam" VI 8166
                                                                       ESSCO
                                               Sample from Raytheon
 The temperature run was made with stacked disks at 8.5 GHz. The thickness
  shown is the stack height divided by the number of pieces and includes
  expansion due to trapped decomposition gases.
                                                                    Excess phase
  T°C
           K
                 D.F. Thick., om Attan., db Insertion loss, db
                                                                     shift (deg.)
    25
         2.943
                 .0158
                           .063
                                      .00789
                                                                        .058
                                                     .0587
    49
         2.843
                 .0216
                           .0664
                                      .0114
                                                     .0621
                                                                        .065
         2.835
                                      .0155
                                                                        .067
    73
                 .0292
                           .0669
                                                     .0665
  107
         2.84
                 .047
                           .0677
                                      .0252
                                                     .0779
                                                                        .071
  129
         3.032
                 .0304
                           .0696
                                                                        .086
                                      .0169
                                                     .0343
  163
         3.129
                 .0764
                           .0676
                                      .0410
                                                                        .088
                                                     .1112
  179
         2.744
                 .0723
                           .0754
                                      .0432
                                                     .1018
                                                                        .090
  198
         2.748
                 .0569
                           .0784
                                      .0355
                                                     .0988
                                                                        .103
  233
         1.664
                 .0283
                           .1139
                                      .0253
                                                     .0446
                                                                        .091
  245
         2.165
                 .0251
                           .0909
                                      .0180
                                                     .0559
                                                                       .096
  258
         2.817
                 .0426
                           .0760
                                      .0258
                                                     .0900
                                                                        .098
  272
         3.02
                 .0527
                           .0731
                                      .0307
                                                     .1042
                                                                        .102
  300
         3.09
                 .0418
                           .0735
                                      .0246
                                                     .1040
                                                                       .107
```

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General Electric
"Lexan" General Purpose Grade, clear
                                                                                          $.5x10
                                           106
                                                                                  2.773
                                                                          2,780
                                           2.971
                           3,003
                                            .00049
                                                   .0111
                                                           .0103
"Lexan" 500, polycarbonate
                                                       24 GHz
               R.T. 8.5 GHz
                                                                  D.F
                                          T°C
                                                       K
                        D.F.
               K
                                                                 .00625
                       .00568
                                           24.4
                                                    2.881
            2.921
                                                                 .00734
                                           62.3
                                                    2.872
                                                                 .00739
                                                    2.871
                                           68.3
                                                                             General Electric
"Nory1" (s)
                                           Moryl N300
                                                                            109
                                                                                   3x10<sup>9</sup>
                                                                                           8.5×109
                                            106
                            104
                                    105
            102
                    103
                                                                                           2.720
                                                                                   2.723
                            2,767
                                    2.751
                                            2.736
            2.791
                                                                    .00266
                                                                             .00336
             .00324
                    .00357
                                            Moryl RK300
                                                                                           3.050
                                            3.020
.00573
                                                   2.982
                                                           2.976
                                                                   3.065
                                                                           3.062
                                                                                   3.057
                                    3,048
                    37117
                            3,061
            3.3,44
                                                                                            .00091
                                                                            ,00578
                     .00669
                            .00697
                                            Noryl 101240
                                                                                           3.046
                                                                                   3.052
                                            2.960
            3.059
                            3,002
                                    2,981
                    3.034
                                                    .00289
                                                            .00280
                            .00581
                                     .00469
                                             .00385
   Note: Electric field 5e perpandicular to faces of injection molded Noryl disks in the frequency range 102 to 108 Hz; at higher frequencies electric field is parallel to faces of disks.
                                                                    G.E. Sample from Sperry
 "Noryl" undesignated
                                       24 °C
                                                                                       14
                                                                         8.5
                                            3
                                                           5
         Freq., GHz
                               1
                                                                                     2.648
                                                                       2.652
                                                          2.65
                                           2.65
                             2.66
               K.
                                                                         .00396
                                                                                      .0058
                                                           .0036
                                            .00313
               D.F.
                               .0020
                                                                             General Electric
 PPO-534-861, polyphenylene oxide
                                                        24 GHz
                R.T. 8.5 GHz
                                                                     D.F.
                                                        ĸ
                                           T°C
                         D.F
                K
                                                                    ,00251
                         .00181
                                             25
                                                     2.628
              2.635
                                                                    .00257
                                            62.2
                                                    2.622
                                                                    .00246
                                            102.6
                                                    2.616
                                                                    .00253
                                                    2.599
                                            139.7
                                                                    .00256
                                            145.5 2.598
                                                                    .00269
                                            184.5
                                                     2.515
                                                                    .00231
                                             25
                                                     2.564
                                                                             General Electric
  RTV's
                                24°C
                                         8.5 GHz
                                             D.F.
                              K
            #60, red
                            3.736
                                           .0172
            #630, grey 3.016
                                           .0199
```

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Marco 28C
                                                        Grace Industries
                      R.T.
                            8.5 GHz
                                                        Sample from Sperry
                      ĸ
                              D.F.
                    2.929
                              .0164
    Sample #1
    Sample #2
                    2.880
                              .0114
Polyethylene with olive drab pigment
                                                        Hardigg Industries
     24 GHz 23°C
                     K = 2.29
                                D.F. = .00062
Radome fabrics
                                                         Hoover Industries
                     22 °C
                              8.5 GHz
  Averages for three samples:
                              D.F.
                                        Thickness, cm
                    2.889
        Grey
                              .0172
                                            .059
        White
                    2.895
                              .0174
                                            .056
Polyethylene with 20 wt% gamma ferric oxide (<1\mu) R.T.
                                                                 Hellerbond
  Frequency, GHz
                            1
                                      1.685
                                               2,45
                                                         3
  Dielectric Constant
                            2.6605
                                              2.6576
                                                        2.6520
  Dielectric Loss Tangent
                             .0025
                                                .0018
                                                         .0015
  Magnetic Permeability
                            1.1163
                                               1.1099
                                                        1.0860
                                      1.113
  Magnetic Loss Tangent
                             .01287
                                       .0389
                                                .0684
                                                         .0821
Hercules PC-072-2 polypropylene
                                                                 Hercules
  R.T. 8.5 GHz
                             24 GHz
                                     T°C
                                              K
                                                     D.F.
   K = 2.532
                                      25
                                            2.525
                                                    .00206
   D.F. = .00217
                                      62.1 2.511
                                                    .00222
                                      97.8 2.483
                                                    .00232
                                     133.2 2.441
                                                    .00246
                                      25
                                           2.532
                                                    .00208
"Hycar" E4109
                                                                      Hycar
                                 8.5 GHz
                                                        Samples from Raytheon
                       T°C
                               K
                                      D.F.
                                                           K
                                                                     D.F.
                        22
     Sample A
                             1.191
                                     .0020
                                            Sample B
                                                         1.178
                                                                   .00196
                       125
                             1.201
                                     .0062
                                                         1.186
                                                                   .0054
                        25
                             1.190
                                     .0021
                                                         1.175
                                                                   .0020
"Thermocomp" DF1008
                                                 Liquid Nitrogen Proc. Corp.
    40% glass fiber reinforced polycarbonate 23°C
           Freq. MHz
                           1
                                      10
                                               100
           K
                          3.81
                                     3.79
                                               3.73
           D.F.
                           .00704
                                      .0084
                                                 .00864
LNP-OF-1006 polyphenylene sulfide
                                                                        LNP
                  R.T.
                         8.5 GHz
                                              24 GHz
                    K
                          D.F.
                                       T°C
                                                K
                                                        D.F.
                  3.762 .00406
                                        25
                                              3.709
                                                       .0055
                                              3.722
                                        58.6
                                                       .0058
                                        85.8
                                              3.715
                                                       .0063
                                              3.712
                                       107.5
                                                       .CO67
                                       135.8
                                              3,677
                                                       .0078
                                        25
                                              3.706
                                                       .0053
```

		R.T. 8.	5 GHz		24 (GHz			
		K :	D.F.	T°C	K	D.	F.		
	3	.613 .00	0763	25	3.532	2 .00	87		
				61.8					
				83.8					
				112.	3.516	-			
				126.8					
				138.3					
"Loctite	" LI-260		2	4°C			Loctite	e Corp.	•
Freq., Hz	100	1 k	10 k	100 k	1 M	10 M	8.5 G	14 G	24 G
к ¹	4,568	4,459	4.319	4.093	3.716	3.356	2.409	2.404	2.394
K 11	.0851	.0888	. 127	.200	.243	.230	.072	.0683	.0645
tan & (D.F.		.0199	.0295	.0489	.0653	.0684	.0299	.0284	.02695
o mho/cm	4.74E-1		7.09E-10	1.11E-8	1.358-7	1.28E-6	3.41E-4	5.31E-4	8.31E-4
Bondex 4	20					1		tite Co	
Samv1	~ #1	8.5 GHz		mple #2	13 68	Sampi	es from	n Speri	ry
T°F	.e #1 K	D.F.		mpte #2 n.GHz	3	5	8.5	14	ı.
1 F	K			q. Gnz	3	5		Τ,	•
74	2.855	.0128		K	3.07	3.05	3.027	2.95	58
139	2.90	.0168		D.F.	.025	.026	.027	.02	263
204	2.89	.0191							
"Merlon"	1799 po	lycarbona	te		1	Mobay Ch	emical	Corp.	
			oven d	ry					
1000/T	T, DEG.C	FREQ.,HZ	к	t	K2	TAN	DELTA	SIGM	A,MHO/CM
3.3653	24.0	20.	2.8		0.001810		00630		113E-13
3.3653 3.3653	74.0 24.0	50. 100.	2.8 2.8		0.001600		00556 00503		455E-13 886E-13
3.3653	24.0	200.	2.8		.001821		00629		235E-12
3.3653	24.0	500.	2.8		0.002099		00725		299E-12
3.3653	24.0	1000.	2.9		0.002241		00771 00863		450E-11
3.3653 3.3653	24.0 24.0	2000. 5000.	2.9 2.9		0.002507		01146		854E~11 465E~11
3.3653	24.0	10000.	2.9		0.004523		01558		128E-10
3.3653	24.0	20000.	2.8		0.005672		01960		022E-10
3.3653	24.0	50000.	2.8	• •	0.008290		02891		027E-09
3.3653 3.3653	24.0 24.0	100000.	2.8 2.8		0.010191 0.022129		03590 07807		618E-09 294E-07
3.3653	24.0	300000.	2.8		0.015637		05438		061E-08
3.3653	24.0	3000000.	2.8	45	0.026918	0.0	09462	0.44	864E-07
3.3653	24.0	6000000.	2.8		0.027568		09529		894E-07
3.3653 3. 3653	24.0 24.0	9500000. 30 000000.	2.9 2.8	-	0.029700 0.029737		1022B		675E-06 562E-06
								7. 10	

"Merlon	1799 pc	olycarbonate	.15% w	ater			Mobay
1000/T	T,DEG.C	FREQ.,HZ	K 1	K	2	TAN DELTA	SIGMA,MHO/CM
3.3653	24.0	5.	2.939	0.00	2726	0.004074	
3.3653	24.0	10.	2.941	0.00		0.001271 0.000962	0.10378E-13
3.3653	24.0	20.	2.934	0.00		0.000757	0.15721E-13
3.3653	24.0	50.	2.935	0.00		0.000553	0.24685E-13
3.3653	24.0	100.	2.933	0.00		0.000498	0.45090E-13 0.81140E-13
3.3653	24.0	300.	2.930	0.00		0.000575	0.28082E-12
3.3653	24.0	1000.	2.931	0.00	2294	0.000783	0.12743E-11
3.3653	24.0	3000.	2.931	0.00		0.001081	0.52803E-11
3.3653	24.0	10000.	2.927	0.004	4844	0.001655	0.26908E-10
3.3653	24.0	20000.	2.925	0.00	6437	0.002200	0.71524E-10
3.3653 3.3653	24.0 24.0	50000.	2.922	0.009		0.003235	0.26260E-09
3.3653	24.0	100000.	2.920	0.01		0.004233	0.68661E-09
3,3653	24.0	1000000.	2.896	0.024		0.008489	0.13655E-07
3.3653	24.0	300000. 3000000.	2.916	0.01		0.006066	0.29485E-08
3.3653	24.0	9500000.	2.875	0.029		0.010233	0.49029E-07
3.3653	24.0	30000000.	2.848 2.837	0.03		0.011265	0.16936E-06
	4		2.031	0.02	328	0.009984	0.47214E-06
"Merlon	1799 po	olycarbonate	.40% w	ater			Mobay
1000/T	T,DEG.C	FREQ.,HZ	K 1	K2	!	TAN DELTA	SIGMA,MHO/CM
3.3653	24.0	30000000.	2.831	0.035	201	0.012434	0 E0000
3.3653	24.0	9500000.	2.878	0.038		0.013329	0.58668E-06 0.20245E-06
3.3653	24.0	6000000.	2.889	0.038		0.013172	0.12687E-06
3.3653	24.0	16000000.	2.868	0.036		0.012657	0.32273E-06
3.3653	24.0	3000000.	2.907	0.037		0.013053	0.63245E-07
3.3653	24.0	30000C.	2.952	0.023	151	0.007842	0.38585E-08
3.3653	24.0	1000000.	2.928	0.032	768	0.011191	0.18205E-07
3.3653	24.0	100000.	2.973	0.015	012	0.005049	0.83403E-09
3.3653	24.0	50000.	2.951	0.011	321	0.003837	0.31447E-09
3.3653	24.0	20000.	2.979	0.007		0.002482	0.82140E-10
3.3653 3.3653	24.0	10000.	2.987	0.005		0.001853	0.30754E-10
3.3653	24.0 24.0	5000.	2.987	0.004		0.001376	0.11414E-10
3.3653	24.0	2000. 1000.	2.982	0.003	-	0.001049	0.34762E-11
3.3653	24.0	500.	2.985 2.987	0.002		0.000877	0.14544E-11
3.3653	24.0	500.	2.989	0.002		0.000843	0.69976E-12
3.3653	24.0	200.	2.983	0.001		0.000806	0.66963E-12
3.3653	24.0	100.	2.988	0.001		0.000656 0.000651	0.21751E-12
3.3653	24.0	100.	2.989	0.001		0.000612	0.10814E-12
3.3653	24.0	50.	2.988	0.001		0.000612	0.10170E-12 0.50805E-13
3.3653	24.0	20.	2.990	0.002		0.000692	0.23000E-13
Napthal	ene C ₁₇	o ^H 8				MIT Materia	al. Science
		Freq., GHz	1	1.7	3	8.5	14
220			-	d. T f	,		
23°C s	0110	K				2.76	2.75
		D.F.				.00016	00025
82°C 1:	iquid	K	2.53	2.53	2.53		2.47
	-	D.F.	.0001	.00022	.0005	2	.00115
		~	1000			-	· • • • • • • • • • • • • • • • • • • •

Laminato	ed polyp	ropylene 24	GHz 24°	°c		MI	r,Lincoln
Thick	ness, cm	K	D.F.	•			
.4: .7: .80	51	2.27 2.28 2.27	.0010 .0016 .0037				
RX-18 pc	olymethy	1pentene					Mitsui
			Samp	oles from	Naval	Underwater	Sys. Cen
Colo	or	Freq., M	Iz 400	1000	3000	8515	21°C
	, 1977 , 1978	K D.F. K	2.132 .00041		2.127 .00043	.00054	
none,	, 1976	D.F.				2.133 .00063	
Yello	w	K				2.132	
Red		D.F. K D.F.				.00062 2.1325	
Dark	Blue	K K				.00062 2.134	
I i abt	Blue	D.F.				.00064	
DISH	. bide	K D.F.				2.130 .00063	
TPX Nat	ural					***************************************	Mitsui
T°C F	req.,GHz	1	1.685	2.45	3	5	8.5
25	K	2.122	2.122	2.121	2.121	2.120	2.120
75	D.F. K	.00059	.00061	.00063	.00063		
13	D.F.			2.092 .00067			
125	K			2.060	•		
175	D.F. K			.00071			
173	D.F.			.00076			
"Texin"	355D n	atural, poi] ***********				
	333B, II	acurar, po.	Lyurechani	e Oven Dry	,	Mobay Chem	ical Corp.
1000/T	T, DEG.C	FREQ.,HZ	K 1	ка	t	TAN DELTA	SIGMA,MHO/CM
3.3653 3.3653	24.0	5.	5.827	0.493		0.084651	0.13701E-11
3.3653	24.0 24.0	10. 20.	5.720 5.624	0.321 0.233		0.056253	0.17876E-11
3.3653	24.0	50.	5.562	0.177		0.041447 0.031828	0.25902E-11 0.49172E-11
3.3653 3.3653	24.0 24.0	100. 200.	5.498	0.158		0.028829	0.88052E-11
3.3653	24.0	500.	5.466 5.325	0,172 0,170		0.031628 0.032080	0.19208E-10
3.3653 3.3653	24.0	1000.	5.258	0.170		0.032350	0.47453E-10 0.94492E-10
3.3653	24.0 24.0	2000. 5000.	5.204	0.169		0.032595	0.18846E-09
3.3653	24.0	10000.	5.106 5.026	0.17 <i>4</i> 0.169		0.034156 0.033764	0.48443E-09
3.3653 3.3653	24.0	20000.	4.951	0.186	249	0.037615	0.94284E-09 0.20694E-08
3.3653	24.0 24.0	50000. 100000.	4.892 4.765	0.197		0.040345	0.54820E-08
3.3653	24.0	1000000.	4.446	0.207 0.248		0.043581 0.055915	0.11537E-07 0.13810E-06
3.3653 3.3653	24.0 24.0	300000.	4.624	0.223	435	0.048325	0.13810E-06 0.37239E-07
3.3653	24.0	3000000. 9500000.	4.238 4.059	0.261 0.285		0.061662	0.43558E-06
3.3653	24.0	30000000.	3.825	0.329		0.070401 0.086210	0.15081E-05 0.54957E-05

"Texin"	355	D				24% wa	ter				Moba	У
1000/T	T, DE	G.C	FRE	Q.,HZ		K 1	К2		TAN (DELTA	SIGMA,M	HD/CM
3.3653 3.3653		1.0		1000. 300.		529 653	0.197 0.199		0.03		0.10945 0.33301	
3.3653		.0		100.		821	0.226		0.03		0.12595	
3.2653		1.0		3000.		409 252	0.200		0.03		0,33385 0,11620	
3.3653 3.3653		1.0 1.0		0000. 0000.		157	0.215		0.04		0.23916	
3.3653		1.0		0000.		041	0.235		0.04		0.65386	
3.3653		0	10	0000.		946	0.236		0.04		0,13114	
3.3653		1.0		0000.		569	0.270		0.05		0,15034	
3.3353	- 24			0000.		771 354	0.249		0.05		0,41599 0,46426	
3.3653 3.3653		1.0 1.0		0000.		159	0.298		0.07	• • •	0.15756	
3.3653		1.0		100.		744	0.198		0.03	4555	0.11026	
3.3653	24	1.0		50.		865	0.240		0.04		0.66766	
3.3653		3.0		20.		990	0.358		0.05		0.39778 0.24008	
3.3653	24	1.0		10.	0.	088	0.432	1-41	0.07	0369	Ų. 2400C	, E - 1 1
"Texin"	355	D			1	.14% w	vater				Mobay	,
1000/T	7,D	EG.C	FRE	Q.,HZ		K1	K2	!	TAN	DELTA	SIGMA,	MHO/CM
3.3653	2	4.0	3000	00000.	4	. 0 44	0.396			8006	v.6606	
3.3653		4.0		00000.		.328	0.378			37390	0.1996	
3.3653 3.3653		4.0 4.0	•	00000.	-	.471 .603	0.369			32618 78168	0.5996	
3.3653		4.0		ებები.		.151	0.317			31671	0.7059	
3.3653		4.0		00000.		.151	0 292			6847	0.3253	7E-07
3.3653		4.0		20000.		.708	0.280			19068	0.1556	
3.3653		4.0		500 00.		.379 .573	0.261			18534 13922	0.72519 0.2719	
3.3653 3.3653		4.0 4.0		20000. 10000.		.673	0.239			12267	0.1332	
3.3653		4.0		5200.		.185	0.24	-		39204	0.6735	
3.0653		1.0		2000.		.883	0.272			16255	0.3023	
3.3653		4.0		1000.	-	.964	0.32			54652 59834	0,1810 0,1182	
3.3653 3.3653		4.0 4.0		500. 200.		.095 .246	0.69			0727	0.7684	
3.3653		4.0		100.		.407	1.15			79529	0.6390	
3.3653	2	4.0	10	00000.		987	0.34			70842	0.1923	
3.3653		4.0		50.	_	.660	1.66			50363	0.4631	
3.3653 3.3653		4.0		50. 20.		.640 .157	1.94			93261 79605	0.5409	
3.3653		4.0		10.		.634	7.58			57773	0.4211	
Polysu]	lfons	e bos	rd					Non	plex I	ivisio	on, UOP I	inc.
	T OC	Freq.,	GH∠	1	2.45	3	5	8.5	14	24		
	23	tmi A)	2.981	2.978	2.977	2,975	2.96f .00539	2.950 .00560	2.945 .00573		
	51	ton A	i	2.983 .00412	2.976 .00484	2,975 .00523	2.973 .00568	2,954 .00595	2.946 .00623	2,940 .00669		
	100	tan '		2.984 .00458	2.982 .00548	2.980 .00585	2.976 .00634	2.953 .00704	2.943 .00734	2.940 .00760		
	150	ten d	,	2.965 .99428	2.943 .00552	2.961 .00603	2.958 .00664	2.948 .00766	2.943 .00812	2.935 .00877		
	175	tan d	,	2.948 .00370	2,946 ,0050n	2.945 -00546	2.941 .00623	2.934 .00762	2.928 .00872	2.921 .00948		
	150	tan /	١.	2.952 .00362	2,952 ,00474	2.951 .00526	2.930 .00594	2.946 .00495	2.940 .00725	2.934 .00784		
	100	tan 4		2.953 .00357	2,952 ,00458	2.951 .60489	2,949 .00547	2.942 .00629	2.936 .00660	2.931 .00680		
	50	tan (,	2.959	2,957	2.957	2.755 .00501	2.940	2,935 .90570	2.926 .00574		
	23	tan		2.959	2.758 .00408	2.956	2.934	1.937	2.935	2.930		

Temperature Runs to the Liquid State at 2.45 Ghz on ten materials Phillips Petroleum Co.

							D I COLOZECIM DO
#5226	3			#5226	4		
		ass fill					mineral filled
polyp	henyle	ne sulli	de	polyp	heny1e	ne sulfi	de
T°C	ĸ	D.F.	Thick.,cm	T°C	K	D.F.	Thick.,cm
24.5	4.12	.00438	1.506	24	4.33	.0059	1.574
47	4.11	.00464	1.510	64	4.35	.0088	1.379
85	4.10	.00505	1.517	92	4.38	.0112	1.578
112	4.05	.0057	1.523	112	4.34	.0126	1.579
155	4.04	.0083	1.528	143	4.29	.0132	1.590
205	4.00	.0106	1.545	178	4.26	.0134	1.599
242	3.95	.0128	1.591	209	4.11	.0134	1.654
				229	3.97	.0128	1.732
#5226	5			#5226	6		
Type	R-10 g	lass & m	ineral filled	Miner	al fil	led poly	sulfone
			fide color cmpd.				
22	4.88	.0037	1.513	23	3.37	.00517	1.670
55	4.89	.0040	1.517	67	3.38	.00595	1.676
76	4.90	.0042	1.519	93	3.38	.0064	1.680
99	4.92	.00514	1.522	120.6	3.33	.0062	1.683
118	4.91	.0059	1.521	153	3.23	.0065	1.709
152	4.90	.0076	1.528	176.5	2.91	.0097	1.908
171	4.90	.00816	1.531	206	2.55	.0224	2.377
210	4.88	.00936	1.547				
240	4.83	.0105	1.573				
#5226	7			#5226	8		
polys	u1fone			Glass	fille	d polybu	tylene
				terep	hthala	te	
23	3.06	.0049	1.678	24	3.49	.00645	1.664
	3.07	.0055	1.680	54	3.47	.0110	1.676
89.6	3.04	.0060	1.690	87	3.47	.0203	1.688
113	3.00	.0057	1.700	114	3.48	.0352	1.705
157	2.91	.0060	1.735	145	3.50	.0448	1.726
174	2.62	.0084	1.884	175	3.65	.0772	1.776
204	2.30	.0209	2.34	197	3.94	.0937	1.772
				235	4.24	.1152	1.818
#5226				#5227	0		
polyb	utylen	e tereph	thalate	Glass	fille	d polyac	etal
	2.97	.0050	1.707		3.26	.0292	1.728
	2.98	.0102	1.721		3.49	.0309	1.761
	2.96	.0189	1.737	87	3.61	.0649	1.785
	2.96	.0435	1.770	118.5		.0563	1.799
139	2.99	.0596	1.771	146	3.99	.0511	1.812
165	3.14	.0836	1.768	179	4.24	.0491	1.943
199	3.58	.1172	1.778	199	4.04	.0445	2.098
230	3.9 0.	.1383	1.849				

Ph111	.ips pl	astics,	continu	ed						
#5227	1 polya	cetal			#	52272	2 poly	propy	1ene	
T°C	K '	D.F.	Thick.	, cm	T	°C	ĸ	D.	F.	Thick., cm
21	3.08	.0338	1.679			24.2	2.242	.00	041	1.684
	3.21	.0623	1.685				2.240		045	1.684
75	3.39	.0805	1.700			56	2.233	.00	051	1.685
111	3.60	.0741	1.713			96	2.195		054	1.702
142	3.82	.0605	1.728		1	30.7	2.159		069	1.729
184	3.99	.0489	1.980			58	2.014		079	1.846
196	4.08	.046	1.755		1	87	1.779		07.7	2.559
Cross	-linked	polyet	hylene C	L-100	_	_			*.	Phillips
					S	amp1	e molde	ed by	Herdi	.88
24 0	GHz 23°	'd K =	2.229	D. 7	00056					
		rber Mi								Raytheon
		Corning		2.0	45 GHz					
		e, 60 w	•		•		ratio			
T°C	K'	tan δ	μ¹/μ _ο	tan $\delta_{\mathtt{m}}$	T°C	ĸ'	tai	nδ	μ ' /μ _c	, tan $s_{ m u}$
22*	4.47	.0127	, 9985	.491	22*	5.79	9 .03	129	1.553	.8996
24	4.35	.0123	J. 014	. 483	23	5.7	2 .0	117	1.554	.894
65	4.27	.0110	.940	. 498	62	5.6	3 .0:	11.2	1.502	.881
88	4.20	.0110	.901	.432	92	5.60	0.0	109	1.397	7 .903
113	4.15	.0111	.837	. 454	95	5.60	0.0	109	1.386	.902
127	4.12	.0117	.822	.391	120	5.5	6 .0:	129	1.323	.911
156	4.09	.0129	.817	.295	128	5.5	.O.	137	1.309	.902
179	4.05	.0138	.813	.232	153	5.5	0 .0	150	1.21	L .924
210	4.00	.0152	.840	.1535	184	5.4		1.59	1.130	.926
241	3.95	.0180	.891	.052	220	5.4		195	1.027	
259	3. 92	.0190	.913	.033	233	5.3		214	1.012	2 .944
290	3.87	.0212	.984	.0081	272	5.3		265	.896	
22	4.37	.0114	1.012	. 494	298	5.3		285	.797	
						5.9		127	1.480	
* :	in room	temp. s	ample ho	lder, ot						
"Plex	xiglass'	' V811-1	.00, poly	methy 1me	thacry	late	, oven	dry	Rhom	& Haas Co.
1000/	T T,DE	G.C FRE	Q.,HZ	К1		K2	,	'AN DE	ELTA	SIGMA, MHO/CM
			.4.1	.,,						01 am/(m/o/ o/m
3.36	53 24	.0 3000	0000.	2.607	0.0	25432		.0097	755	0.42386E-06
3.36	53 24	.0 950	0000.	2.596	0.0	15776	C	. 6060	78	0.83264E-07
3.36			0000.	2.639		35585		0.0134		0.59308E-07
3.36 3.36			00000.	2.681 2.664		51897 40346).0193).0151		0.86496E-08 0.22415E-07
3.36			00000.	2.705		57965		0.0214		0.32203E-08
3.36			0000.	2.742		67078		0.0244		0.18633E-08
3.36 3.36			0000.	2.782 2.849		76921 82731).027().029(0.85468E-09 0.45962E-09
3.36			0000.	2.849		B4718		0.029		0.47065E-09
3.36		. 0	5000.	2.889	0.0	96873		0.033		0.26909E-09
3.36			3000.	2.921		05489		0.036		0.17582E-09
3.36 3.36		, 0 , 0	1000. 500.	3.000 3.032		27622 42581		0.042		0.70901E-10 0.39606E-10
3.3€	53 24	.0	200.	3.100	0.1	59903	(0.051	582	0.17767E-10
3.36		. 0	100.	3.168		47102		0.046		0.81723E-11
3.36 3.36		.0	50. 20.	3.255 3.408		57021 68988		0.048		0.43617E-11 0.18554E-11
3.36		.0	10.	3.494		72959		0.049		0.96088E-12
3.38	53 24	.0	5.	3.569	0.1	74577	•	0.048	921	0.48494E-12
3.36 3.36		1.0 1. 0	3.	3.636		3B368 43764		0.038		0.23061E-12
3.00	24		2.	3.731	0.1	43764	•	0.038	J3V	0.15974E-12

'Plexiglas:	" conti	nued			R	nom & Haas
			.27% water	Molded	by Eastman,	from MIT ME
1000/T	T,DEG.C	FREQ.,HZ	K 1	К2	TAN DELTA	SIGMA,MHQ/CM
3.3653	24.0	9500000.	2.596	0.034817	0.013414	0.18376E-06
3.3653	24.0	300000 0 .	2.654	0.041893	0.015783	0.69822E-07
3.3653	24.0	300000.	2.731	0.059684	0.021858	0.99473E-08
3.3653	24.0	1000000.	2.673	0.050151	0.018762	0.27862E-07
3.3653	24.0	100000.	2.755	0.067682	0.024566	0.37601E-08 0.20229E-08
3,3653	24.0	50000.	2.799	0.072824	0.026018 0.027854	0.20225E-00
3.3653	24.0	20000.	2.843	0.079186 0.085537	0.030081	0.47520E-09
3.3653	24.0	10000.	2.844	0.103130	0.035441	0.17188E-09
3.3653	24.0	3000.	2.910 3.014	0.122055	0.040498	0.67808E-10
3.3653	. 24.0	1000. 1000.	3.014	0.121073	0.040165	0.67263E-10
3.3653	24.0 24.0	300.	3.061	0.143380	0.046533	0.23897E-10
3.3653 3.3653	24.0	100.	3,220	0.171322	0.053137	0.95179E-11
3,3653	24.0	50.	3.289	0.150950	0.045894	U.41931E-11
3.3653	24.0	20.	3.407	0.161970	0.047547	0.17997E-11
3.3653	24.0	10.	3.539	0.172468	0.048727	0.95815E-12
3.3653	24.0	5.	3.632	0.172526	0.047507	0.47924E-12
3.3653	24.0	3.	3.658	0.147920	0.040435	0.27390E-12
3.3653	24.0	2.	3.797	0.140221	0.036928	0.15580E-12
			1.5% water			
1000/T	1,DEG.C	FREQ.,HZ	К1	К2	TAN DELTA	SIGMA,MHD/CM
3.3653	24.0	10.	4.117	0.241926	0.058758	0.13440E-11
3.3653	24.0	10.	4.147	0.222634	0.053684	0.12369E-11
3.3653	24.0	20.	4.029	0.218649	0.054270	0.24234E-11
3.3€33	24.0	50 ,	3.871	0.296526	0.053346	0.57368E-11
3.3653	24.0	100.	3.768	0.194061	0.051509	0.10781E+10
3.3653	24.0	200.	3.672	0.178341	0.048567	0.19816E-10
3.3653	24.0	500.	3.532	0.187601	0.073107	0.52111E-10
3.3653	24.0	1000.	3.454	0.169185	0.048989	0.93992E-10
3.3653 3.3653	24.0 24.0	2000.	3.121	0.149799	0.043784	0.16644E-09
3.3653	24.0	5000. 10000.	3.341 3.290	0.129041	0.038624	0.35845E~09
3.3653	24.0	20000.	3,243	0.116235 0.107560	0.035327 0.033162	0.64575E-09
3.3653	24.0	50000.	3,191	0.098730	0.030953	0,11951E-08
3.3653	24.0	100000.	3.162	0.095400	0.030169	0.274395-08 0.53000E-08
3.3653	24.0	500000.	3.008	0.085960	0.027987	0.23850E-07
3,3653	24.0	1000006.	3.029	0.078446	0.025898	0.435816-07
3.3653	24.0	300000.	3.095	0.088521	0.028603	0.14754E-07
3.3653	24.0	3000000.	2.976	0.068226	0.022924	0.11371E-06
3.3653	24.0	9500000.	2.935	0.056405	0.019220	0.29769E-06
3.3653	24.0	30000000.	2.874	0.046728	0.016257	0.77880E-06

Richo 31001 polyurethane

Richo Plastics

Sample from Sperry

8.5 GHz 23°C K = 2.979 D.F. =.0186

"Duro	ld"	5650	M-5

"Duroid" 5870

Rogers

Rogers

8.5 GHz 21 °C

E perpendicular hot pressing direction K = 2.660 D.F. = .00242 E parallel " " K = 2.558 D.F. = .00206

•

8.5 GHz 21 °C E parallel to sheet

 Thickness, inch
 X
 D.F.

 1/16
 2.42
 .0019

 .010
 2.33
 .0019

"Duroid" 5870M-1 Rogers

E perpendicular HPD 2.443 .00207 E parallel HPD 2.317 .00138

"Duroid" 5870M Rogers

In Room Temperature Sample Holder

		Rotation (degrees)	к	tan δ	
1 pc. full thickness	Face 1	0	2.630	.00287	E 4
•		90	2.495	.00237	E //
	2	0	2.632	.0031	EL
		90	2.484	-00207	E //
	pc. 1/ p	oc. 2 0	2.592	.00283	E 🚣
	- · •	90	2.452	.00213	E //

Temperature run pc. 2/pc. 1

	E			E //	
T°C	ĸ	tan δ	Thickness (cm)	κ	tan δ
23.1	2.594	.00287	1.8583	2.462	.00256
50	2.592	.00306	1.8619	2.464	.00226
97	2.593	.00229	1.8670	2.460	.00203
160.	2.591	.00209	1.8681	2.452	.00199
205	2.17	.00159	1.8722	2.425	.00129
246	2.571	.00182	1.8734	2.419	.00131
300	2.563	.001.86	1.8805	2.405	.00131
350	2.395	.00239	2.0639	2.258	.00130
395	2.242	.00251	2.2581	2.159	.00100
468	2.088	.00289	2.5177	1.989	.00112
504	1.828	.00396	3.2300	1.722	.00339
528	1.095	.00155	4.7506	1.017	.0195

OTADGEATERED						
		Room	Temperatu	re		
Material #	Freq., GHz	.4	1	3	8.5	
0200	к	2.265	2.265	2.264	2.264	
8240	d.f. K d.f.	.00029 2.247 .00029	.00026 2.247 .00029	2.246	.000275 2.246 .00027	
"Epon" 828 100 phs re	sin, 80 pts ha	rdener, 1	pt accele	rator C-3)	Sample fr	Shell om Brunswick
		2.45 GHz	23°C	,	K	D.F.
	30 min. after : 5 hrs at 23°C, 47 hrs " Then 95 hrs at Then 80 hrs at Cured 1 hour at	40°C	ome bubble es	s	3.907 3.710 3.310 3.165	.198 .214 .152 .0756 .0533
Various Plas				Samples	formed by	Sperry
	A11	at 8.5 GH	z, R.T.	κ 2.850	tan δ .0209	
Cycloaliphat		_		2.861	.010	
Polyester, o	ting, face face Laminac			2.850 2.911	.0086	
"Epon" 815,				2.60 13.9	.0074 .007	
Ciba 2790,	clear HY 917			2.87 12.9	.0135 .0095	
ъс. 7521				13.0	.0045	
Hetron 92FS	1			13.5	.0095	
"Stafoam"				1.035	.00103	•
Richo 90-57	8 + 34-841			1.042		
Rigid polyu (Same a	irethane foam it 1 GHz)			1.036 1.039		
Rigid poly	rethane foams:				, 3	(rr. 1) / 3 m
	esignation Leng	gth,cm .35 1 .55 1	1225	D.F. .00145 .00155	gm/cm ³ - .096	(K-1)/den. - 1.28
87	2	.10 1		.00214 .00229	.1189	1.34
V12	2	.30	.2872	.00390 .00362	.2056	1.41
V16	2	. 32	1.3271	.00456 .00460	.2398	1.35
V20	2	.13	1.3948 1.3895	.00455	.2941	1.32

8.5 GHz R.T.

Thickness, inch K D.F.

1/32 2.35 .0004

1/16 2.34 .00033

"Mindel"	Stabili:	zed basic	polys:	ulfone	1976		Union	Carbide Corp.
	T, DEG.C	FREQ.,HZ	•	K 1	К2	TAN.	DELTA	SIGMA,MHO/CM
1000/T	I, DEG. C	PREWITE	•	**		TAN	0111	JI GIRK, INTO/ CM
3.3484	25.5	. 1000000.	3	.607	0,013891	0.00	3851	0.77170E-08
3.3484	25.5	9500000		.584	0.014416	0.00		0.76082E-07
3.3484	25.5	30000000	_	.579				
3.3484	25.5	100000.		.627	0.008946		2466	0.49697E-09
3.3484	25.5	10000		.639	0.008157		2242	0.45315E-10
3.3484	25.5	1000		.651	0.010085		2762	0.56027E-11
3.3484	25.5	100.		1.671	0.012933		3523 3813	0./1852E-12 0.39008E-12
3.3484	25.5	50.		683	0.014043 0.019363		5340	0.53787E-12
3.0945	50.0	50		3.626 3.614	0.016199		4482	0.89995E-12
3.0945	50.0	100		3.590	0.011298		3147	0.62767E-11
3.0945 3.0945	50.0 50.0	10000	_	3.572	0.008738		2446	0.48544E-10
3.0945	50.0	100000	•	3.558	0.007548		2121	0.41932E-09
3.0945	50.0	1000000		3.538	0.010719		3030	0.59551E-08
3.0945	50.0	9500000		3.520	0.013302	0.00	3779	0.70207E-07
3.0945	50.0	30000000		3.512				-
2.6799	100.0	30000000		3.387				
2.6799	100.0	9500000		3.390	0.009495		2801	0.50114E-07
2.6/99	100.0	1000000		3.425	0.006362		1858	
2.6799	100.0	100000		3.431	0.006911		02014	0.38395E-09 0.54349E-10
2.5799	100.0	10000		3.441	0.009783		028 43 04444	0.85459E-11
2.6799	100.0	1000	-	3.461	0.015383 0.025626		07301	0.14237E-11
2.6799	100.0	100		3.510 3.528	0.030249		07574	0.84025E-12
2.6799		50 50		3.526	0.046422		13050	0.12895E-11
2.3632		100		3.550	0.037887		10671	0.21049#-11
2.3632 2.3632		1000		3.504	0.022269		06356	0.12372E-10
2.3632		10000	-	3.497	0.013270		03795	0.73723E-10
2.3532		100000	-	3.458	0.008736		02526	0.48531E-09
2.3632		1000000		3.456	0.005919	0.0	01712	0.328858-08
2.3632		9500000		3.436	0.006981	0.0	02032	0.36846E-07
2,3632	150.0	30000000	١.	3.424				
2.2314		30000000		3.434				
2.2314		9500000		3.444	0.006878		01997	0.36303E-07
2.2314		1000000		3.458	0.007112		02056	0.39510E-08 0.55169E-09
2.2314		100000		3.480	0.009930		02854 048 25	0.93595E-10
2.2314		10000		3.492 3.522	0.016847 0.027321		07758	0.151786-10
2.2314		1000		3.570	0.054329		15217	0.30183E-11
2.2314 2.2314		50		3.596	0.076612		21303	0.21281E-11
2.2314	1/5.9	50	, .	3.550	0.070012	•••		V. W. 1.
At 2	5°C afte	r cemper	ature r	un:				
				2	3.5	6		9.5
Freq.,		.5	1			-		00326
Tan de	lta .	00336	00370	.00369	.00350	.00339	9 .	00326
Microw	ave data	1:						
Freq.,	GHz	.15	.3	1	2.45	3		8.5
к		3.63	3.63	3.63	3.626	3.62	4 :	3.618
	_		.00320	.00362		.0041		00477
Tan de	TES	. 00300	.00320	.00302	.00703	***	•	

"Radel" p	ooly; hen	/lsulfo	ne	1	976		Union Carbide			
1000/T	T,DEG.C	FREQ.	,HZ	К1	К2	TAN	DELTA	SIGMA,	MHO/CM	
3.3428 3.3428 3.3428 3.3428 3.3428 3.3428 3.3428 3.3428	26.0 26.0 26.0 26.0 26.0 26.0 26.0		00. 00. 00. 60. 50.	3.090 3.067 3.054 3.138 3.138 3.139 3.130 3.119 3.111	0.015613 0.013474 0.011929 0.003346 0.003189 0.003530 0.003654 0.004941	0.0 0.0 0.0 0.0 0.0	05053 04393 03906 01066 01016 01124 01167 01584 03051	0.8673 0.7111 0.1988 0.1858 0.1063 0.9804 0.2029 0.2745	96-07 16-06 86-12 06-12 56-13 96-11 16-10	
3.0945 3.0945 3.0945 3.0945 3.0945 3.0945 3.0945 2.6799	\$0.0 50.0 50.0 50.0 50.0 50.0 50.0	300000 95000 10000 1000 100 100	00. 00. 00. 00. 00. 00. 50.	3.034 3.056 3.070 3.082 3.088 3.092 3.114 3.116 3.069	0.016283 0.014325 0.012026 0.006560 0.004375 0.003760 0.003895 0.004514 0.010899	0.0 0.0 0.0 0.0 0.0 0.0	05366 04687 03917 02161 01417 01216 01251 01449	0.2713 0.7560 0.6681 0.3700 0.2430 0.2088 0.2164 0.1253 0.3027	9E-06 5E-07 2E-08 2E-09 3E-10 6E-11 1E-12 8E-12	
2.6799 2.6799 2.6799 2.6799 2.6799 2.6799 2.3632 2.3632	100.0 100.0 100.0 100.0 100.0 100.0 150.0	10 1000 1000 10000 95000 300000 95000	00. 00. 00. 00. 00.	3.063 3.064 3.060 3.032 3.025 3.022 2.986 2.997 3.003	0.008544 0.004451 0.003849 0.904239 0.006789 0.011622 0.014829 0.011814 0.008740	0.0 0.0 0.0 0.0 0.0 0.0	02769 01453 01258 01398 02244 03346 04967 03943	0.4746 0.2473 0.2138 0.2354 0.3771 0.6134 0.2471 0.1969 0.4612	0E-11 5E-10 9E-09 4E-08 1E-07 5E-06 1E-06 6E-07	
2.3632 2.3632 2.3632 2.3632 2.3632 2.3632 2.2314	150.0 150.0 150.0 150.0 150.0 150.0 175.0	1 10 100	00. 00. 00. 00. 50. 00.	3.002 2.985 3.008 3.017 3.030 3.027 2.996 2.989	0.005359 0.004182 0.004254 0.006471 0.017789 0.029222 0.010348 0.005134	0.0 0.0 0.0 0.0 0.0	001785 001401 001414 002145 005871 009655 003454	0.2977 0.2323 0.2363 0.3594 0.9882 0.8117 0.5748 0.2880	6E-09 4E-10 9E-11 5E-12 2E-12 8E-11 2E-10	
2.2314 2.2314 2.2314 2.2314 2.2314 2.2314	175.0 175.0 175.0 175.0 175.0 175.0		00. 00. 00. 50.	2.985 2.983 2.981 2.959 3.001 3.016	0.004093 0.004754 0.007016 0.009583 0.047240 0.078053	0.0 0.0 0.0	001371 001594 002354 003239 015739 025882	0.2273 0.2641 0.3702 0.1597 0.2624 0.2168	0E-08 7E-07 2E-06 5E-11	
Freq.,	C after	.1	.5	n: 1	2	3.5	6	9.5	16	
Tan de		0355	.00502	.00539	.00562	_	.00513		.00446	
	ave data				.00302	• 00223	•00313	********	100440	
Freq.,		.15	.3	1	2	.45	3	8.	5	
K.	3	.15	3.15	3.15	3.	145	3.14	3.1	3	
Tan de	1ta .0	0422	.00466	.00535	.00	583	.00590	.0063	7	

"Rade1"	5000, ba	itch 6	1977			Union Carbide
1000/1	T, DEG.C	FREQ.,HZ	K1	K2	TAN DELTA	SIGMA, MHD/CM
3.3462	25.7	30000000.	3.225	0.015655	0.004855	0.26091E-06
3.3462 3.3462	25.7	9500000.	3.249	0.017758	0.005466	0.93720E-07
3.3462	25.7	1000000.	3.280	0.019903	0.006068	0.11057E-07
3.3462	25.7 25.7	500000.	3,289	0.018275	0.005556	0.50765E-08
3.3462	25.7	3500000.	3.273	0.019114	0.005840	0.37166E-07
3.3462	25.7	6000000.	3.267	0.018102	0.005540	0.60341E-07
3.3462	25.7	2000000. 100000.	3.278	0.020383	0.006217	0.22647E-07
3.3462	25.7	10000.	3.314	0.012325	0.003719	0.68470E-09
3.3462	25.7	1000.	3.324	0.006728	0.002024	0.37377E-10
3.3462	25.7	100.	3.333 3.337	0.005138	0.001542	0.28547E-11
3.3462	25.7	50.	3.340	0.004497 0.004390	0.001347	0.24983E-12
3.3462	25.7	10.	3.344	0.004597	0.001315	0.12194E-12
3.0945	50.0	10.	3.373	0.003845	0.001375	0.25536E-13
3.0945	50.0	50.	3.367	0.003845	0.001140	0.21362E-13
3.0945	50. 0	100.	3.365	0.004294	0.001275 0.001276	0.11922E-12
3.0945	50.0	1000.	3.365	0.004493	C.001276	0.23854E-12
3.0945	50. 0	10000.	3.361	0.005586	0.001662	0.24961E-11
3.0945	50.0	100000.	3.349	0.008392	0.001662	0.31031E-10
3.0945	50.0	1000000.	3.330	0.016008	0.004808	0.46620E-09 0.88935E-08
3.0945	50.0	3500000.	3.308	0.018926	0.005720	0.36800E-07
3.0945	50.0	6000000.	3.304	0.019846	0.006007	0.56154E-07
3.0945	50.0	9500000.	3.257	0.019724	0.006056	0.10410E-06
3.0945 2.6799	50.0	30000000.	3.230	0.017414	0.005391	0.29023E-06
2.6799	100.0	30000000.	3.277	0.017188	0.005246	0.28647E-06
2.6799	100.0	95000CO.	3.303	0.016053	0.004961	0.84724E-07
2.6799	100.0	6000000. 3500000.	3.312	0.014460	0.00436B	0.48201E-07
2.6799	109.0	1000000.	3.316 3.322	0.013026	0.003928	0.25327E-07
2.6799	100.0	100000.	3.329	0.009055 0.005697	0.002726	0.50305E-08
2.6799	100.0	10000.	3.344	0.003697	0.001711	0.31651E-09
2.6799	100.0	1000.	3.346	0.003191	0.001349	9.25054E-10
2.6799	102.0	100.	3.346	0.004024	0.000954 0.001202	0.17728E-11
2.6799	100.0	50.	3.348	0.004350	0.001299	0.22355E-12
2.6799	100.0	10,	3.352	0.004761	0.001421	0.12082E-12 0.26452E-13
2.3632	150.0	10.	3.337	0.008127	0.002436	0.45151E-13
2.3632 2.3632	150.0	50.	3.326	0.005039	0.001515	0.13997E-12
2.3632	150.0	100.	3.325	0.004616	0.061388	0.25643E-12
2.3632	150.0 150.0	1000.	3.324	0.004200	0.001264	0.23331E-11
2.3632	150.Q	10000.	3.318	0.005729	0.001726	0.31828E-10
2.3632	150.0	100000.	3.312	0.004871	0.001471	0.27064E-09
2.3632	150.0	9500000	3.299 3.304	0.008096	0.002454	0.44980E-08
2.3632	150.0	30000000.	3.235	0.012436 0.015230	0.003764	0.65635E-07
2.1135	200.0	30000000.	3.204	0.017966	0.005016	0.27050E-06
2.1135	200.0	9500000.	3.259	0.013099	0.005608	0.29944E-06
2.1135	200.0	1000000.	3.257	0.008395	0.004019 0.002578	0.69133E-07
2.1135	200.0	100000.	3.274	0.011336	0.003463	0.46642E-08
2.1135	200.0	10000.	3.292	0.006291	0.001911	0.62976E-09 0.34950E-10
2.1135	200.0	1000.	3.312	0.007955	0.002402	0.44192E-11
2.1135	200.0	100.	3.314	0.022555	0.006806	0.12530E-11
2.1135 2.1135	200.0	50.	3.318	0.037448	0.011285	0.10402E-11
2.0074	200.0 225.0	10.	3.335	0.129655	0.038878	0.72030E-12
2.0074	225.0	10.	4.254	1.648727	0.387569	0.91596E-11
2.0074	225.0	50. 100.	3.708	0.455797	0.122933	0.12661E-10
2.0074	225.0	1000.	3.579 3.401	0.345433	0.096506	0.19191E-10
2.0074	225.0	10000.	3.401	0.104960	0.030863	0.58311E-10
2.0074	225.0	100000.	3.268	0.044307 0.021754	0.013377	0.24615E-09
2.0074	225.0	1000000.	3.240	0.021754	0.006656	0.12085E-08
2.0074	225.0	9500000.	3.202	0.018617	0.005378 0.005815	0.967926-08
2.0074	225.0	30000000.	3.148	0.019601	0.005815	0.98257E-07
			.		4.400220	0.32668E-0 6

"Radel	" 50 0 0, d	continued					
T°C	Freq.,GH:	z 1	1.685	2.45	3	5	8.515
						,	0.313
25	K	3.195	3.190	3.186	3.182	3.170	3.155
	D.F.	.00547	.00533	.00594		.00646	.00654
75	K	3.200	3.193	3.187	3.183	3.171	3.157
	D.F.	.0065	.00646	.0067	.0074	.0080	.00757
1.25	K	3.197	3.191	3.182	3.178	3.169	3.195
	D.F.	.0074	.0072	.0077	.0086	.0094	.00875
175	K	3.194	3.190	3.181	3.177	3.166	3.141
,	D.F.	.00805	.00795	.00835	.0092		
200	ĸ	3.199	3.193			.010	.0098
200	D.F.	.0084		3.180	3.175	3.161	3.120
	D. F.	.0064	.0083	.0088	.0096	.0103	.0102
"Udell	" P1700.	Blend 63-	72	1977			Union Carbide
1000/					K2	TAN DELTA	
,	. ,,,,,,,,	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		•	***	INN USEIA	SIGMA, MNO/CM
3.36					003836	0.001215	0.21313E-13
3.369 3.369					003579 003723	0.001135	0.99417E-13
3.36					003624	0.001181 0.001149	0.20683E-12 0.20131E-12
3.369	53 24.0			39 0.	004013	0.001279	0.22296E-11
3.36			3.1	29 0.	005502	0.001759	0.30567E-10
3.36					010105	0.003240	0.56139E-09
3.369 3.369					015610 015480	0.005043 0.005025	0.86721F-08
3.36					009535	0.003:06	0.81701E-07 0.15892E-06
3.09			3.0		009711	0.003 57	0.16185E-06
3.09					015347	0.004975	0.80997E-07
3.09					011903	0.003(44	0.66125E-08
3.09					005793 003908	0.001868 0.001857	0.32186E-09
3.09	45 50.0				002879	0.000324	0.21711E-10 0.15996E-11
3.09	45 50.0	0 100	3.1	23 0.	002834	0.000307	0.15742E-12
3.09			3.1	26 0.	002814	0.000300	0.78171E~13
3.09 2.67				27 0.	002999	0.000059	
2.67					005021 003440	0.001611 0.001706	0.27895E-13 0.95564E-13
2.67	99 100.0	0 100			003318	0.001688	0.18434E-12
2.67					000283	0.000041	0.15746E-12
2.679 2.679					003210	0.0010.16	0.17833E-10
2.67					004087 006812	0.0013/2 0.002209	0.22706E-09 0.37843E-08
2.67					015220	0.004948	0.37843E-08
2.67		0 30000000	3.0	64 0.	014844	0.004844	0.24740E-06
2.35 2.36					007800	0.002545	0.13000E-06
2.36					009555 005506	0.003113 0.001789	0.50491E-07 0.30586E-08
2.36					003295	0.001068	0.30986E-08
2.36		10000	3.0	89 0.	003178	0.001029	0.17657E-10
2.36					003490	0.001129	0.19390E-11
2.36 2.36					004438 005444	0.001430 0.00:756	0.24657E-12
2.36					008402	0.001756	0.15121E-12 0.46679E-13
2.23). 3.1	23 0.	024379	0.007807	0.13544E~12
2.23					012030	0.003865	0.33417E-12
2.23 2.23					010603	0.003424	0.589082-12
2.23					004452 005330	0.001441 0.001727	0.24735E-11 0.29611E-10
2.23					002816	0.000916	0.15645E-09
2.23					003813	0.001244	0.21184E-08
2.23 2.23					010316	0.003401	0.54445E-07
2.11					012438 018076	0.004114	0.20730E~06
2.11					016358	0.005895 0.005312	0.30127E-06 0.86331E-07
2.11		1000000	3.1	02 0.	019015	0.006130	0.10564E-07
2.11					040219	0.012840	0.22344E-08
2.11 2.11					105181	0.032752	0.58434E-09
2.11					253232 517254	0.074187 0.131319	0.14068E-09 0.28736E-10
2.11	35 200.0	50			636457	0.150959	0.28738E-19 0.17679E-10
2.11	35 200.6	9 10	4,9		980310	0.196988	0.54462E-17
				50			

"Udell" P1700, continued									
T°C Fr	eq.,GHz	: 1	1.685	2.45	3	5	8.515		
25	K	2.995	2.993	2.991	2.990	2.986	2.980		
	D.F.	.00435	.0047	.0050			.00608		
75	K	2.993	2.991	2.988	2.987	2.982	2.976		
	D.F.	.00497	.0053	.0049			.00661		
125	K	2.984	2.983	2.979	2.977	2.9 73	2.969		
	D.F.	.00526	.0056	.005		.00676	.00737		
175	K	3.003	2.998	2.983	2.974	2.930	2.856		
	D.F.	.0080	.0083	.0073	.00902	.0087	.00816		
"Ude11"	P8000	(formerly	"Mindel"	')	1977		Union Carbide		
1000/1	T, DEG	.C FREQ.,+	12	K1	К2	TAN DELYA	SIGMA, MHO/CM		
		•				000	21 OWY ! WILD ! CM		
3.3597	24.			850	0.015715	0.004306	0.829396-07		
3.3597	24.			620	0.013623	0.003763	0.22705E-06		
3.3597 3.3597	24. 24.			680	0.016830	0.004573	0.93498E-08		
3.3597	24.			701 722	0.011566	0.003125	0.64255E-09		
3.3597	24.		3.	735	0.009637 0.012112	0.002589	0.53540E-10		
3.3597	24.			756	0.014206	0.003242 0.003782	0.67286E-11		
3.3597	24.			764	0.015360	0.0040B1	0.78920E~12 0.42667E-12		
3.3597	24.			773	0.017836	0.004727	0.99091E-13		
3.0945 3.0945	50.			778	0.022700	0.00600ġ	0.12611E-12		
3.0945	50. 50.			760 753	0.017612	0.004684	0.48922E-12		
3.0945	50.			753 745	0.016253 0.012819	0.004331	0.90296E-12		
3.0945	50.			7 2 7	0.009887	0.003423 0.002653	0.71214E-11		
3.0945	50.			710	0.008623	0.002334	0.54927E-10 0.47904E-09		
3.0945	50.		. 3.	695	0.010598	0.002324	0.58876E-08		
3.0945	50.			651	0.015408	0.004220	0.81320E-07		
3.0945 2.6799	100.			623	0.011837	0.003267	0.19729E-06		
2.6799	100.			631 656	0.012888	0.003549	0.21481E-06		
2.6709	100.			695	0.012966 0.008235	0.003537	0.68429E-07		
2,6799	100.	100000		705	0.008922	0.002229 0.002408	9.45748E-08 0.49569E-09		
2.6799	100.		• •	726	0.012396	0.003327	0.68866E-10		
2.6799 2.6799	100.			742	0.016426	0.004390	0.91257E-11		
2.6799	100.			764 774	0.024341	0.006467	0.13523E-11		
2,6799	100.			8 0 3	0.031256 0.054660	0.008282	0.86823E-12		
2.3532	150.			839	0.092246	0.014374 0.024028	0.30367E-12 0.51248E-12		
2.3532	150.			790	0.044838	0.011829	0.12455E~11		
2.3632	150.0			778	0.032946	0.008719	0.18303E-11		
2.3632 2.3632	150.0			744	0.020960	0.005598	0.11644E-10		
2.3632	150.0			727 706	0.015101 0.012757	0.004052	0.83693E~10		
2.3632	150.6			677	0.008623	0.003442	0.70872E~09		
2.3632	150.0	9500000	. 3.0	652	0.013743	0.002345 0.003763	0.47904E-08 0.72534E-07		
2.3632	150.0	30000000	. 3.0	514	0.017161	0.004749	0.72534E~07 0.28601E~06		
2.2314 2.2314	175.0			503	0.009362	0.002599	0.15603E-06		
2.2314	175.0		• • •	5 3 3 5 6 6 6	0.013707	0.003772	0.72341E-07		
2.2314	175.0			682 697	0.017783 0.020848	0.004830	0.98792E-08		
2.2514	175.0	10000		726	0.026165	0.005639 0.007022	0.11582E-08		
2.2314	175.0	1000	· 3.	761	0.025904	0.006888	0.14536E-09 0.14391E-10		
2.2314	175.0		_	799	0.041062	0.010809	0.22812E-11		
2.2314 2.2314	175.0			312	0.053381	0.014004	0.14828E-11		
2.1135	200.0			365 776	0.092537	0.023944	0.51409E-12		
2,1135	200.0			7 76 5 28	1.172523 0.987350	0.173032	0.65140E-11		
2.1135	200.0	100	. 5.0		0.858599	0.178601 0.168743	0.27426E-10 0.47700E-10		
2.1135	200.0		. 4.:	221	0.401071	0.095028	0.47700E-10 0.22282E-09		
2.1135 2.1135	200.0			392	0.161689	0.041549	0.89827E-09		
2.1135	200.0			. . .	0.073601	0.019537	0.40889E-08		
2.1135	200.0				0.036921 0.030299	0.010025	0.205128-07		
2.1135	200.0				0.022495	0.008377 0.006300	0.15991E-06		
				· · ·		3.400300	0.37491E-06		

"Udell"	P-8000	, cont	inued								
T°C Fx	eq.,GHz	: 1	1.6	85	2.45	3	1	5		8.515	
25 7 5	K D.F. K	3.590 .0041 3.575	3.5 0 .0 3.5	0420	3.556 .0042 3.547		50 0432 542 ,	3.538 .0043 3.527	8	3.527 .00435 3.525	;
125	n.f. K D.f.	.0047 3.562 .0049	1 .0 3.5	049	.0050 3.532 .0053	3. S	05 04 527	.0049 3.511 .0058		.00480 3.486	
175	K D.F.	3.543 .0052	3		3.517 .0060	3.5	00555 510 0063	3.495 .0067		.00576 3.472 .0069)
Printed	Circui	lt Boar	ab:						Uz	nion Car	bide
Polyimi	de lami	lnate,	11848-	12-3			_				_
r°c :	Frag., Hz	10	100	103	104	10 ⁵	10 ⁶	107	108	109	1010
24.2 50	κ tan δ κ	5.141 .00577	5.122 .00510	5.075 .00459	5.044 .00553	4.972 -00994	4.898 .0156	4.789 .0194	4. ú8 . U22	4.65 .0124 4.67	4.57 .0147 4.58
100	tan (K Lan (.0138 4.68	.0196 4.59
150	K tan A									.0144 4.66 .0144	.0229 4.593 .0263
175	κ ten A									4.65 .0143	4.577 .0319
200	k tan /	7.560	5.797 .1488	5.191 .0525	4.988 .0182	. 929 . 00994	4.830 .00736	4.759 .00820	4.71 .0108	4.64 .0138	4.516 .0346
175	k Emn å	5.519 .110	5.149 .0510	4.971 .9215	4.874 .0112	4.815 .00792	4.75 .0065	4.717 .00939	4.68 .01.14	4.63 .0106	4.54 .0314
150	ten 6	5.325 .0534	4.983 .0265	4.884 .0:27	4.814 .00835	4.765 .00624	4.730 .0070	4.675 .00924	4.63 .0113	4.61 .0130	4.55 .0255
100	tan 6	4.951 .0121	4.850 .00844	4.793 .0067	4.750 ,00529	4.717 .00476	4.671 .0066	4,624 ,0104	4.60 .0108	4.58 .0117	4.514 .0212
50	ten 6	4.823 .00547	4.725 .00691	4.709 .00429	4.684 .00411	4.660 .00557	4.609 .00795	4.544	4.50 -0098	4.55 .0097	4.451 .0169
25	κ tan δ	4.786 .00322	4.695 .00389	4.682 .00396	4.659 .00456	4.621 .0069	4.547 .00841	4.503 .010B	4.46 .0110	4.51 .0086	4.413
Poly	olefin,	cross	linked,	11848	-12-2						
т ^о с	Fraq., Hr	10	100	103	104	105	106	107	108	109	1010
24	κ tan δ	2.91 .00322	2.89 .00455	2.869 .0053	2 : 845 . • 00644	2.814 .00668	2.777	2.761 -00735	2.757 .0076	2,847 .00754	2.842 .00664
50	t a n ó									2.860 .0103	2.828 .00807
100	tan ó K									2.845	2.796
175	tan ó «									2.877 .0236 2.861	2.778 .0170 2.759
200	tan 6 K	3.229	3.046	3.002	2.884	2.790	2.755	2.688	2.59	.0276 2.778	.0205 2.756
175	tan 6	.438 3.226	.0633 3.216	.0265 3.045	.0310 2.923	.0134 2.872	.0132 2.812	.0212 2./31	.0272 2.65	.0303 2.779	.0216 2.757
150	tan 6	3.219	.0334 3.067	.0345	.0183 2.936	.013) 2.883	.0177 2.824	.0211 2.740	.0232 2.69	.0248 2.781	.0200 2.782
100	tan ô K tan ô	.0467 3.012 .00247	.0345 3.005 .00417	.0165 2.978 .00#59	.0117 2.931 .0115	.0134 2.874	.0166 2.821	.01 88 2.766	.0211	. 0225 2 . AOS	.0165 2.801
50	r ian d	2.817 2.00650	2.807	2.796 .00554	2.773 .00554	.0128 2.767 .00557	.0137 2.704 .00658	.0139 2.705 .03742	.0136 2.695 .0084	.0130 2.806	.0104 2.802
25	k tan 6	2.824	2,820 .00251	2.814	2.805 .00336	2.789	2.767	2.743	2.73	,00815 2,504 ,00632	.00686 2.802 .00536

Printed	Circui	t Board	ls, con						Ur	ion Ca	rbide
Polysul	fone P-	1700,	11848-	12-1							
r ^o c	Freq., Hu	10	100	103	104	105	106	107	1 0 8	109	1010
24	c tan ô	3.203 .06111	3.186 .00132	3.173 .00157	3.157 .00240	3.152 .00448	3.141 .00610	2.094	3. 16 .: 097	3.043 .0063	3.025 .00652
50	K tan S									3.05 .00702	3.031
100	K tan å									3.05 .00785	3.029 .00878
150	K tan 8									3.06 .0087	3.016 .01154
175	r ten 6									3.03 0095	2.983 .0122
200	r tan ô	5.48 .293	4.30 .186	3.59 .0923	3.35 .0413	3.21 .0199	3.16 .0094	3.13 .0087	3.08 .010	3.92 -(148	2.977 .0132
1.75	« tan s	3.22	3.22 .00756	3.20 .00720	3.14 .00952	3.12 .00342	3.10 .00371	3.09 .00411	3.07 .00 64	3.01 .01962	2.977 .0139
150	κ tan δ	3.21	3.18 .00787	3.14	3.11 ,00407	3,10 .00317	3.09 .00270	3,08 ,00333	3.06 .0052	3.03 .00)82	2.993 .0108
100	K tan ó	3.09	3.08 .00064	3.08 .00057	3.08	3.08 .00094	3.07 .00158	3.07 .00303	3.05 .0042	3.01 .0055	2.977 .00783
50	ĸ tan ô	3.09 .00041	3.08 .00054	3.08	3.08 .00095	3.07 .00141	3.07	3.04 .00352	3.95 .0043	3.00 .0046	2.969 .00609
25	K tan 6	3.097 .00046	3.088 .00066	3.085 .00096	3.060 .00134	3.073 .00160	3.063 .00256	3.056 .00384	3.03 .0039	3.00 .0041	2,966 ,00519
At 24 ⁰	C, 30 Hala,	tan 60	L 6								
Dalarasi	lfone F	_1720	11848	-12-2							
rorysu.	Freq., Hz	10	100	103	104	10 ⁵	10 ⁶	107	10 ⁸	109	10 ¹⁰
24	к	3.252	3.238	3.233	3.222	3.197	3.159	3.141	3.08	3.044	3.032
50	t a n ô K	.00119 3.23	.00144 3.22	.00226 3.21	.00306 3.20	.00446 3.20	.00774 3.17	.00764 3.13	.0061 3.08	.00366 3.050	, 170660 3 . G 34
100	tan ô K	.00127 3.19	.00098 3.18	.00125 3.17	.00162 3.17	.00272 3.15	.00555 3.15	.00795 3.14		.00656 3.05	.0)757 3.015
150	tan ô	.00221 3.27	.00263 3.22		.00170 3.15	.00181	.00287 3.11	,00546 3,10		.0078 3.04	.00726 3,006
24	tan 6	.00491 3.11	.00827	.00777	.00518	.00433	.00379	,00451		.0086	.0115
	K ten 6	.00061	.00081	3.10 .00103	3.10	3.09 .00237	3.08 .00326	3.07 .00389)		
50	k tan 6	3.12 .00051	3.09 .00069	3.09 .00081	3.09 .00111	3.09 .00175	3.08 .00284	3,07 .00375	i		
100	κ tan δ	3.11 .00111	3.09 .00083	3.09 .06073	3.08 .00084	3.08 .00119	3.08 .00196	3.07 .00319	•		
150	ĸ tøn ô	3.24 .00513	3.20 .00958	3.75 .00714	3.13 .00403	3.11 .00371	3.08 .00332	3.08 .00404	•		
	Freq., Hz										
150	tan ó	.00612	.00926								
175	< t a n ô									3.01 ,0093	2.962 .0129
200	K tan ô	4.84	3.84 .1289	3.46	3.28	3.20 .01147	3.16 .00700	3.13	3.08	3.02 .0150	2.942
175	K tan ô	3.26 .00679	3.22	3.19	3.15	3.14	3.11	3.10	3.06	2.95 .00966	2.917 .0123
150	κ t a n δ	3.23 .00617	3.19 .0104	3.14	3.13	3.10	3.10	3.09	3.05	3.00 .00792	2.938 .0102
100				2 10	3 10		2 20		2 04	2 00	2 025

At 200°C, 30 Ms, x = 4.25, tan 6 = .1796

3.11 .00050

3.110 .00045 3.09 .00144 3.06 .00228 3.06 .00334 2.98 .00452 2.932

2.932 .00517

3.10 .00094

3.100 .00135

3.100

Epoxy 2795/2793 with UV stabilizers

Union Carbide Samples from MIT Lincoln Laboratory

3	GHz	R.T.
Stabilizer	κ	tan δ
None	3.11	.0365
Benzotriazole	2.98	.0327
Substituted acrylonitrile	3.09	.0327
Benzidine malonate	3.14	.039
Benzophenone	3.10	.031

Polymer with tungsten wire reinforcement

AFML

	25°C		Te	run 8.5 GHz	
Freq., Hz	κ	tan δ	T°C	K	tan δ
1.00	8.91	.0117	23	3,032	.0241
1K	8.31	.0459	94	3.142	.049
3K	8.02	.0400	101	3,222	.077
10K	7.72	.0487	130	3.294	.106
300K	6.10	.141	150	3.344	.137
1M	5.71	.160	170	3.376	.156
3.5M	4.69	.1.68	208	3.428	.184
30M	3.75	.110			
8.5G	3.034	.0253			

Polyurethane Foam CPR 1057-6.24

Crude oil, low viscosity

Upjohn

MIT

8.5 GHz R.T. K = 1.122 D.F. = .00241

IV. Liquids

T ^O .	c t ^o f	Freq., Hz	102	103	104	10 ⁵	10 ⁶	5x10 ⁶	1.6x10 ⁷	10 ⁹	2.45×10 ⁹	3x10 ⁹
5	8 136	κ tan δ σ	2.667 2.63 3.9E-10	2,456 .332 4.5E-10	.0541	2.327 .0102 1.33E-9	.0038	.0050	2.278 .0073 1.5E-7	2,256 ,0074 9,3 x -6	2,256 ,00495 1,5E-5	2.238 .0052 1.96-5
2	2 72	K	2.643	2.494	2.407	2.376	2.360	2.333	2 309	2 262	2 200	2 272

22 72 K 2.663 2.494 2.607 2.376 7.360 2.333 2.309 2.292 2.290 2.272 2.306 6.5-11 1.5-10 2.35-10 8.K-10 1.5-8 6.9E-8 2.3E-7 4.45E-6 8.7E-6 1.1E-5 2.3E-7 4.4E-8 2.3E-

Crude oil, high viscosity

MIT

C536	(A)40	kan type)	2%					-				
60	140	κ tan δ σ	3,277 .205 5,2E-10	2.903 .37 5.9%-10	2.673 .0705 1.E-9	2.378 .0104 4.98-9	2.548 .0169 2.48-8	2,473 ,019 1,3E-7	2.464 .0173 3.8E-7	2.333 .0000 1.E-5	2,330 .00584 1.85E-5	2.330 .0076 2.95K-5
26	₩2	K ten ô O	3.129 .397 6.9K-11	2.820 .092 1.45-10	2,669 ,0304 4.5K-10	2 606 .0190 2,12-9	2.511 .0190 2.78-8	2,488 ,0154 1,E-7	2.467 .0116 2.5E-7	2.396 .0050 6.65E-6	2,394 ,0040 1,38-5	2.393 .0047 1.9E-5
-16	0	K ten 6	2.811 .0421	2.670 .0275	2.591 .0178 2.68-10	2,339 ,012,6 1,63-9	2.495 .0076	2,492 .0050	2,489 .0032	2.37 .0022	2,3? ,0021	2.37

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